

# HYDROL-INF Modeling System

## User's Manual

Version 6.10



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## **Introduction to HYDROL-INF Version 6.10**

A modified Green-Ampt infiltration-runoff model (Chu and Mariño, 2005) is the central part of the Windows-based HYDROL-INF. A new algorithm is proposed for determining the ponding condition, simulating infiltration into a layered soil profile of arbitrary initial water distributions under unsteady rainfall, and partitioning the rainfall input into infiltration and surface runoff. Two distinct periods, pre-ponding and post-ponding, are taken into account. The model tracks the movement of the wetting front along the soil profile, checks the ponding status, and, in particular, handles the shift between ponding and non-ponding conditions. Furthermore, the model has been extended to complex rainfall patterns that include both wet time periods with unsteady rainfall and dry time periods without rainfall. In addition, the SCS-CN model is also included in the Windows system and some useful hydrologic tools have been developed and incorporated in HYDROL-INF.

Funded by the National Science Foundation, this new version of HYDROL-INF is developed based on the previous one. Particularly, the modified Green-Ampt model in this new HYDROL-INF accounts for the hydraulic effects of surface ponded water on infiltration and unsaturated flow.

### **Acknowledgements**

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It is gratefully acknowledged that permissions to use some published data for estimating model input parameters have been granted by the Food and Agriculture Organization of the United Nations (FAO) and the American Society of Agricultural Engineers (ASAE). Special thanks also to the students in the Watershed Modeling class (CE 476/676) at North Dakota State University and the Hydrology class (NRM 680-A) at Grand Valley State University, for testing the software and providing their feedbacks that have been incorporated in this new version. This software also has been used in the Fluid Mechanics class (CE 309) at North Dakota State University.

### **Notes for Windows Vista and Windows 7 Users**

The compatibility of HYDROL-INF with the Windows Vista and Windows 7 operating systems has been tested. It works well in both new Windows systems. But, two issues have been noticed:

1. Due to the use of higher security technologies, Windows Vista and Windows 7 do not allow any application programs to copy and write files to the folder: C:\Program

Files. Thus, users cannot select any folder within C:\Program Files as their working directory.

2. The Help files in the software require the Windows Help (WinHlp32.exe) program. Starting with the release of Windows Vista and Windows Server 2008, Microsoft has decided to no longer include in WinHlp32.exe as a component of the Windows operating system. For details, please refer to: <http://support.microsoft.com/kb/917607>  
*Solution:* Users need to download and install WinHlp32.exe.

For the Windows Vista operating system, the Windows Help program is available at: <http://go.microsoft.com/fwlink/?LinkID=82148>.

For the Windows 7 operating system, please visit:

<http://www.microsoft.com/downloads/details.aspx?familyid=258AA5EC-E3D9-4228-8844-008E02B32A2C&displaylang=en#top>

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## 1. Installation of HYDROL-INF

Double click the file named “Setup.exe” on the CD drive and then just follow the instructions. After the installation, the HYDROL-INF software can be started from “Start” and “Programs.” One example data file (HYDROL-INF.TXT) is included in the package for testing.

If you are using the Windows Vista or Windows 7 operating system, please install the Windows Help program (WinHlp32.exe) (see the Introduction of this document).

## 2. Instructions for Using HYDROL-INF

Use of the interfaced HYDROL-INF is quite simple, which includes three major steps:

Step 1: prepare all input data via menu “Data” or import data from an existing data file via menu “File-Open Data” (or button Open Data). Then save the data via menu “Save Data” (or button Save Data) or “Save As”.

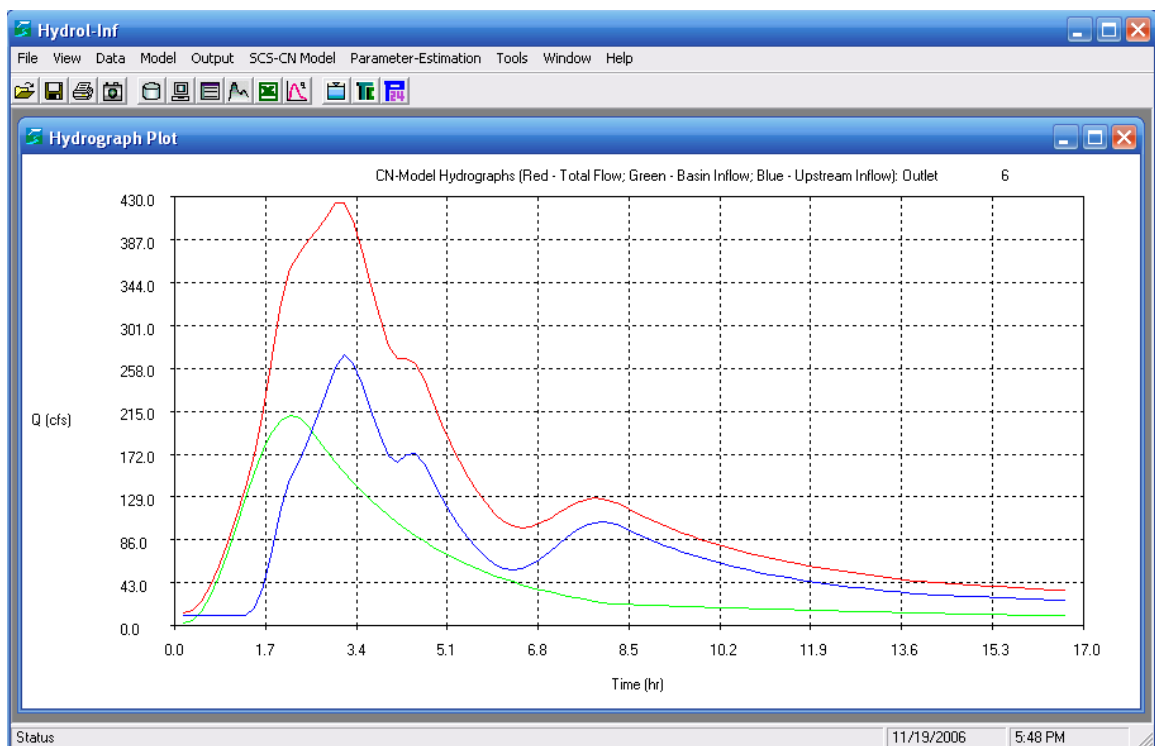
Step 2: check data and run the model via menus “Model-Check Data” and “Model-Run” (or button Check Data and button Run Model). All time-dependent data, such as rainfall, can be input manually or imported from an existing text or excel file. The data can also be exported to a file.

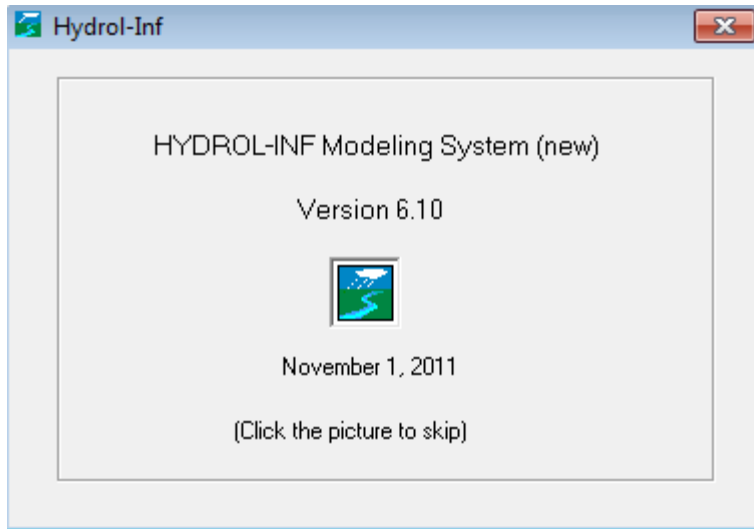
Step 3: Conduct post-processing via menu “Output.” The water mass balance table and graphs of incremental and cumulative rainfall, infiltration, and runoff can be shown via the menu “Water Mass Balance Table” (or button Output Table) and the menu “Rainfall/Infiltration/Runoff Graph” (or button Output Graphs) These outputs can also be exported to Microsoft Excel for further processing (either spreadsheets or graphs) via the menu “Water Mass Balance Excel” (or button Transfer Output to Excel). The graphs can be printed out using menu “File-Print Graph” (or button Print Graph). A graph on the screen can be captured and copied to Clipboard. Additionally, a water table for the surface zone and vadose zone, soil water content, soil water flow velocity, as well as detailed model output information can also be shown via menus. All text-formatted input data and the simulated outputs can be opened and printed via menu “File-Print a Text File.”

### 3. Overview of the HYDROL-INF Interface

#### 3.1. Main Interface

The HYDROL-INF menus are organized according to the three fundamental modeling steps: Data, Model, and Output. The SCS-CN model can be accessed via the menu SCS-CN Model. The menu “Parameter-Estimation” is a special component, which serves as a database and helps users to estimate all input data. It provides explanation and estimation methods for all parameters. It also provides a number of links to some existing databases. Additionally, some hydrologic tools/calculators have been incorporated in the modeling system. The help system covers all information related to the three major modeling steps as well as the HYDROL-INF documentation.





### 3.2. Tool Bar

The buttons in the tool bar (from left to right) are Open Data, Save Data, Print Graph, Screen Capture, Check Data, Run Model, Output Table, Output Graphs, Transfer Output to Excel, Hydrograph, Computation of Measured Flow, and Time of Concentration Calculator.



### 3.3. File

Open Data (button Open Data): Open an existing data file

Save Data (button Save Data): Save the current data

Save As: Save the current data to a user-specified data file

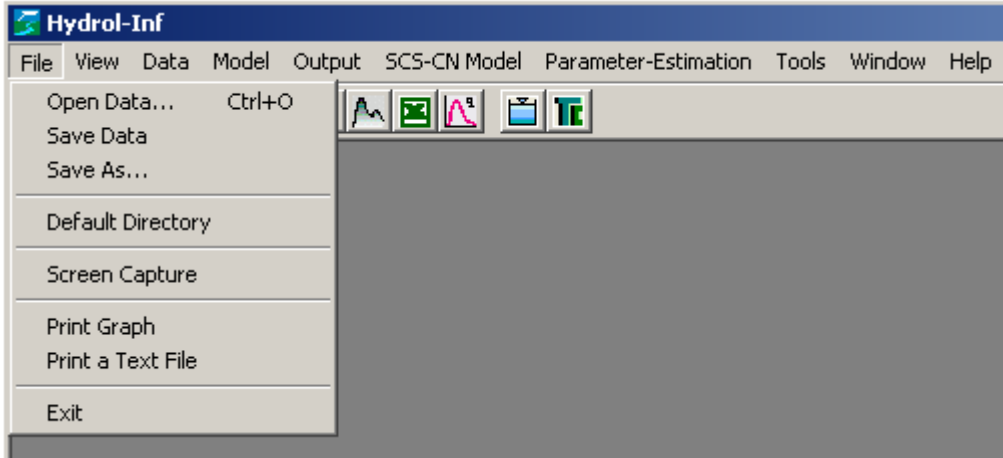
Default Directory: Specify a working directory. The default directory is "C:\HYDROL-INF".

Screen Capture (button Screen Capture): Copy a screen image, such as a graph to Clipboard.

Print Graph (button Print Graph): Print the current graph.

Print a Text File: Open and print a text-formatted input/output file.

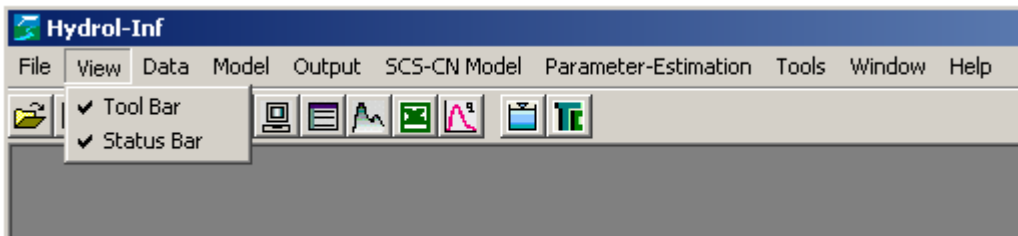
Exit: Exit the HYDROL-INF.



### 3.4. View

Tool Bar: Show/hide the toolbar.

Status Bar: Show/hide the status bar.



### 3.5. Data

Time: Time-related parameters.

Space: Space-related parameters.

Space Parameters

Number of Cells in Each Soil Layer

Thickness of a Soil Layer

Soil: Soil-related parameters.

Saturated Hydraulic Conductivity KS

Effective Hydraulic Conductivity KE

Capillary Head (Suction) HWT

Saturated Water Content WS

Residual Water Content WR

Soil Retention Parameter (n) VN

Soil Retention Parameter ( $\alpha$ ) ALF

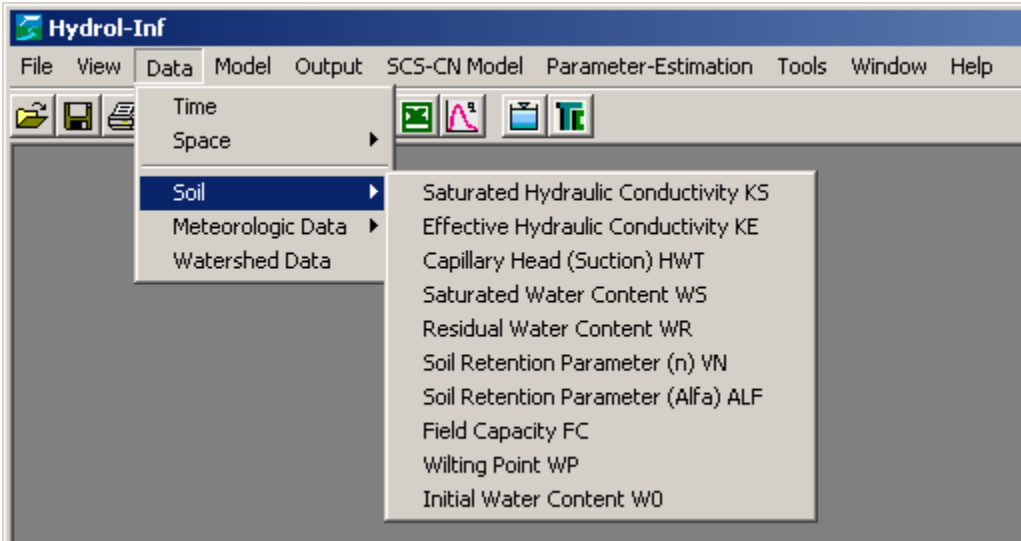
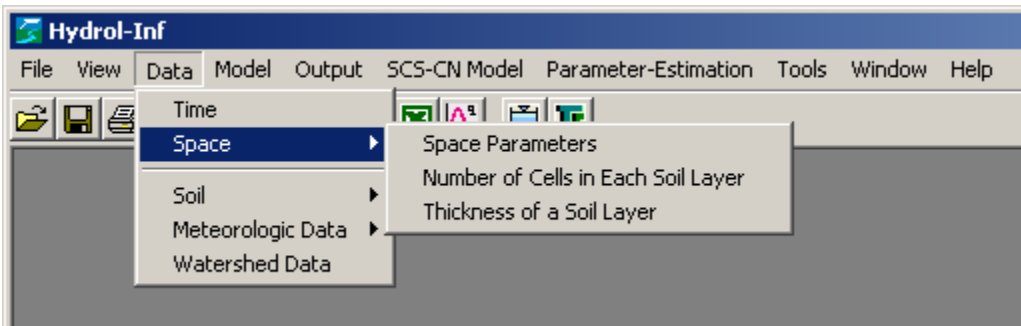
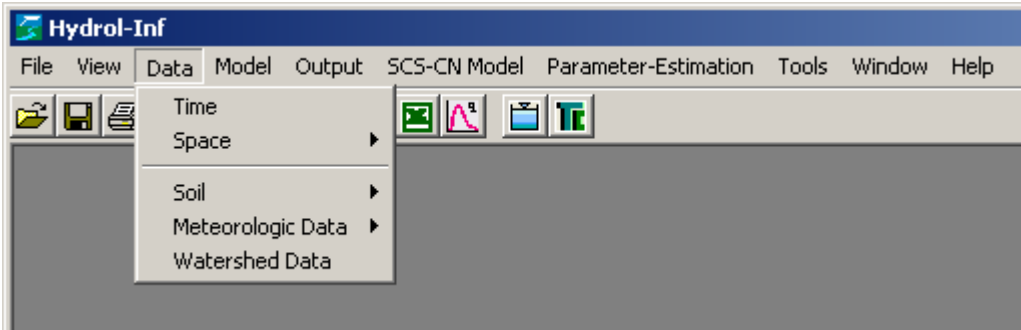
Field Capacity FC

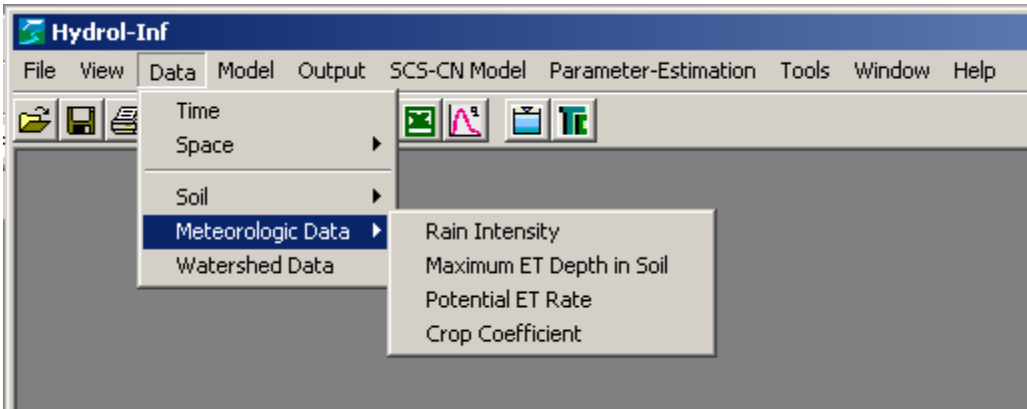
Wilting Point WP

Initial Water Content W0

Meteorological Data:

- Rainfall Intensity (time-dependent data)
- Maximum ET Depth in Soil
- Potential ET Rate (time-dependent data)
- Crop Coefficient (time-dependent data)
- Watershed Data:



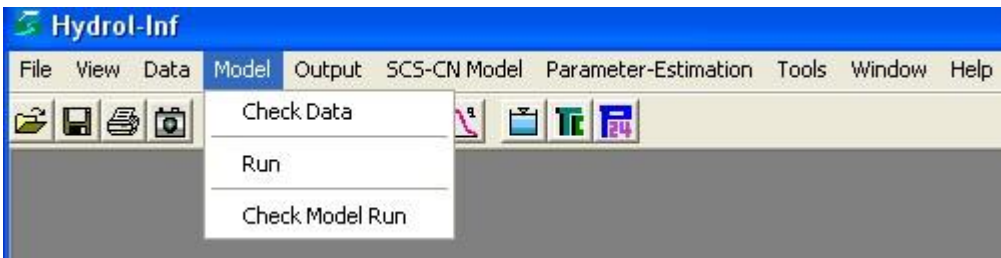


### 3.6. Model

Check Data (button Check Data): Check all input data.

Run (button Run Model): Execute the model.

Check Model Run: Check if the model run is successful.



### 3.7. Output

Water Mass Balance Table (button Output Table)

Rainfall/Infiltration/Runoff Graph (button Output Graphs)

Water Mass Balance Excel (button Transfer Output to Excel)

Water Table for the Surface Zone

Water Table for the Vadose Zone

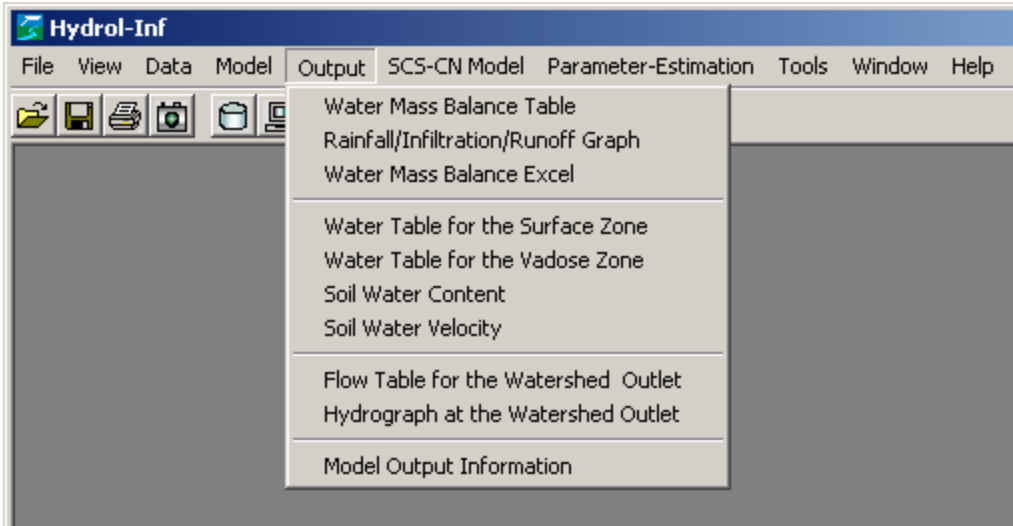
Soil Water Content

Soil Water Flow Velocity

Flow Table for the Watershed Outlet

Hydrograph at the Watershed Outlet

Model Output Information



### 3.8. SCS-CN Model

#### Theory of the CN Method

Equations of the CN Method

CN Tables

P-Q Curves

AMC-I-II-III CN

Composite CN with Impervious Area

#### Data

Import Data (Open)

Working Directory

Unit System Selection

Time Parameters

Watershed Data

Rainfall

Stream Routing Data

Save Data

#### Run CN Model

Check Model Run

#### Output

Water Summary Table

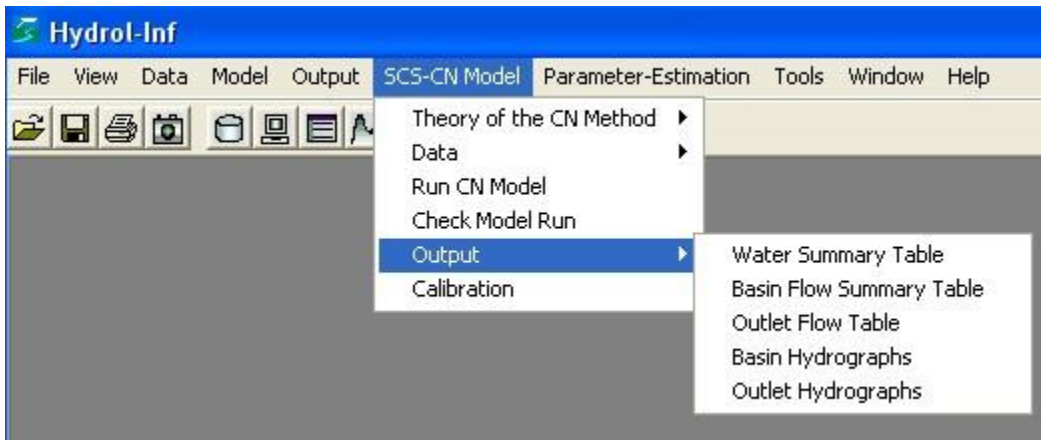
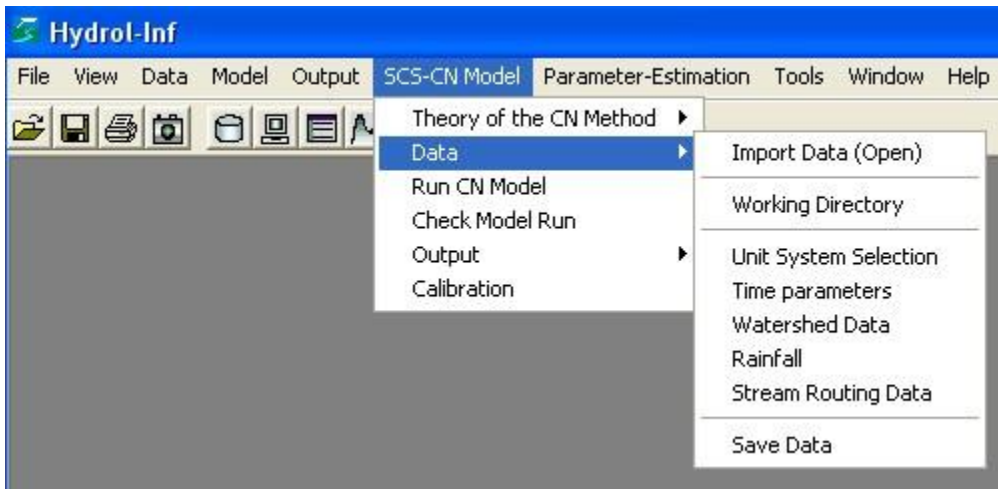
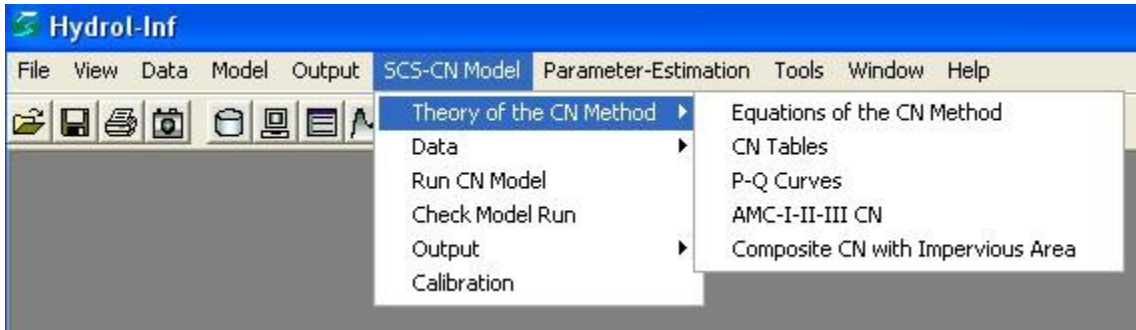
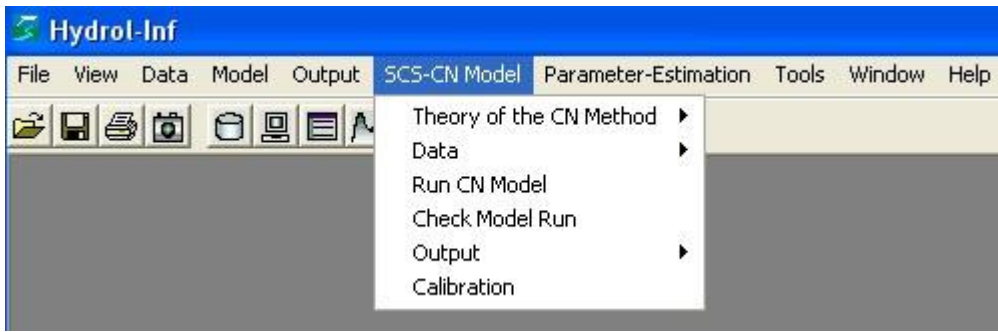
Basin Flow Summary Table

Outlet Flow Table

Basin Hydrographs

Outlet Hydrographs

#### Calibration





### 3.9. Parameter-Estimation

Time Parameters:

Space Parameters:

Soil Parameters:

Saturated Hydraulic Conductivity

Effective Hydraulic Conductivity

Capillary Head (Suction)

Saturated Water Content

Residual Water Content

Soil Water Retention Parameter  $n$

Soil Water Retention Parameter  $\alpha$

Field Capacity

Table

Figure

Wilting Point

Table

Figure

Initial Water Content

Soil Websites

Meteorologic Parameters:

Rainfall Intensity

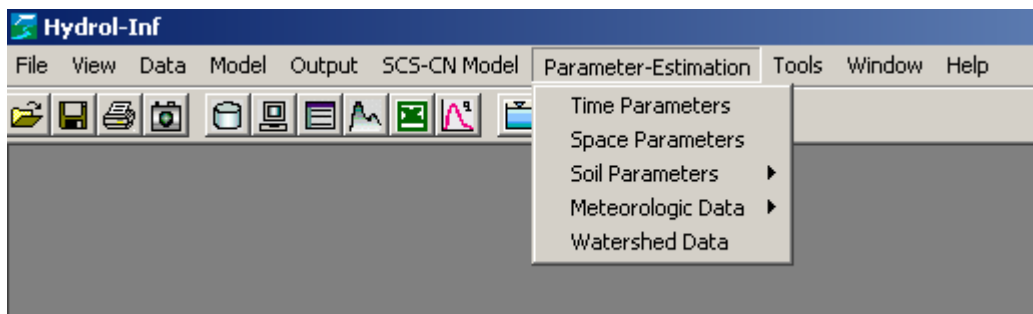
Maximum ET Depth in Soil

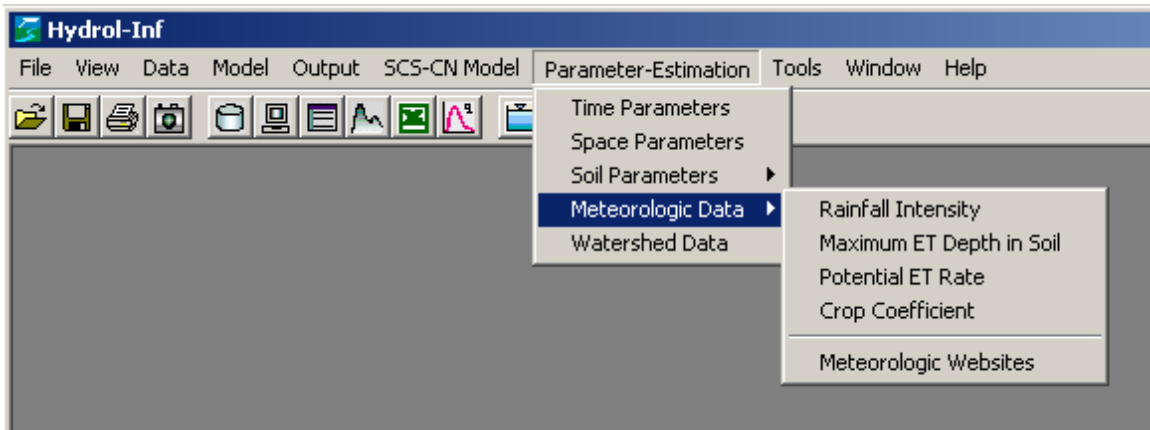
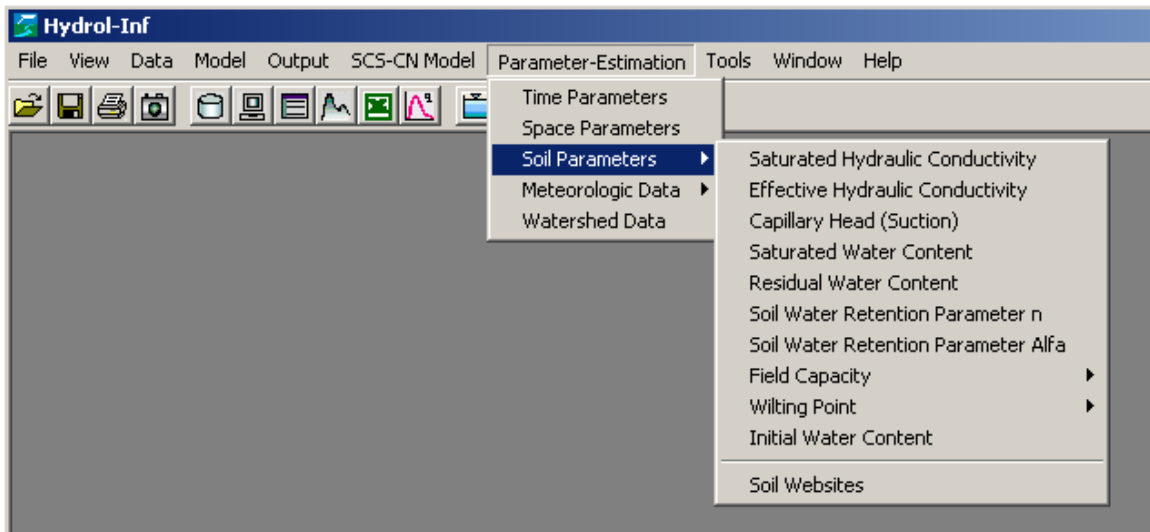
Potential ET Rate

Crop Coefficient

Meteorologic Websites

Watershed Data:



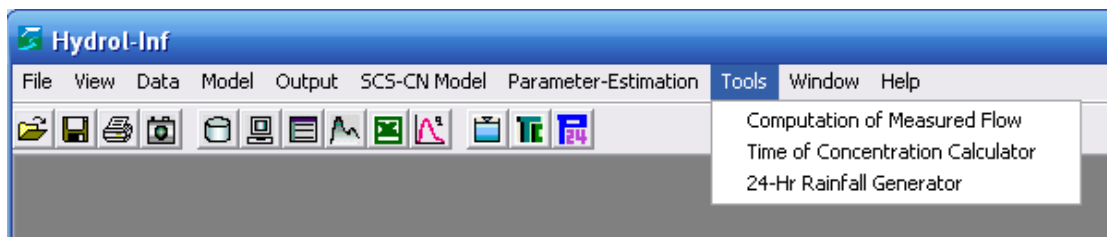


### 3.10. Tools

Computation of Measured Flow (button):

Time of Concentration Calculator (button):

24-Hour Rainfall Generator (button):



### 3.11. Window

New Window:

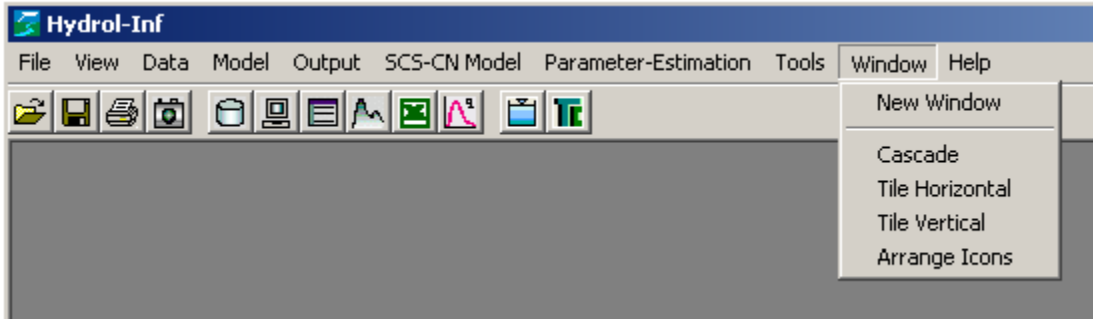
Cascade:

Tile Horizontal:

Tile Vertical:

Tile Horizontal:

Arrange Icons:



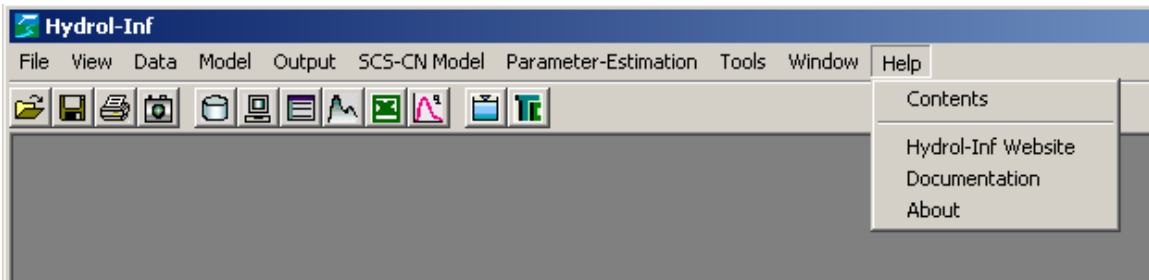
### 3.12. Help

Contents:

Hydrol-Inf Website:

Documentation:

About:



## 4. File Management

### 4.1 Open an Existing Data File

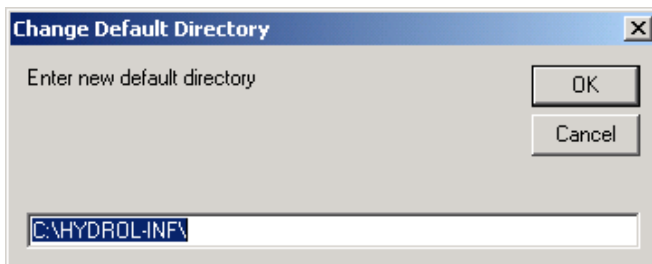
If a data file already exists, you can open the file and import all data through menu File-Open Data or button Open Data in the toolbar. When you open an input data file from a directory, that directory will be automatically set as your working directory.

### 4.2 Save Your Input Data

Save your current input data using menu File-Save Data or button Save Data in the toolbar. The default data file name is “HYDROL-INF.TXT” that will be saved in the default directory (C:\HYDROL-INF) unless you specify a different working directory. Whenever you modify the data, you need to save the data before running the model. The current data can also be saved to a user-specified directory and file name by using menu File-Save As. That directory will be set as your working directory.

### 4.3 Change the Default Directory

The default project directory of HYDROL-INF is “C:\HYDROL-INF\”. You can change it and specify your own project directory through menu File-Default Directory. Then your input data and all output files will be stored in that directory.



### 4.4 Capture a Screen Picture and Copy It to Clipboard

You can make a screen capture and copy the graph/text image to clipboard. Then you can paste it to anywhere, such as your Word Document and Powerpoint presentation.

### 4.5 Print a Graph

After creating a graph (e.g., rainfall/infiltration/runoff graph), you can print it through menu File-Print Graph or button Print Graph in the toolbar. You are also able to select your printer, specify its properties, as well as paper size and orientation. Note that this menu works only when a graph window is active.

### 4.6 Print a Text File (any input data and output files)

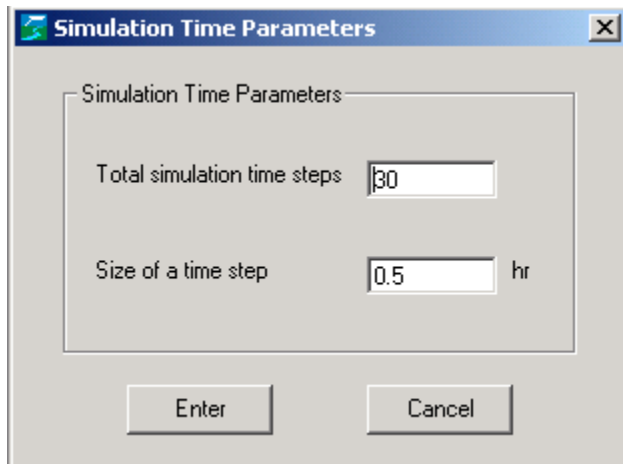
Using menu File-Print a Text File, you can open and print a text file (any input data and output files).

## 5. Input Data and Parameter Estimation

### 5.1 Time Parameters

Total simulation time steps: NT (In the current program,  $NT_{\max}=15000$ )

Size of a time step (hr): DT



The screenshot shows a dialog box titled "Simulation Time Parameters". It contains two input fields: "Total simulation time steps" with the value "30" and "Size of a time step" with the value "0.5" and the unit "hr". At the bottom, there are two buttons: "Enter" and "Cancel".

### 5.2 Space Parameters

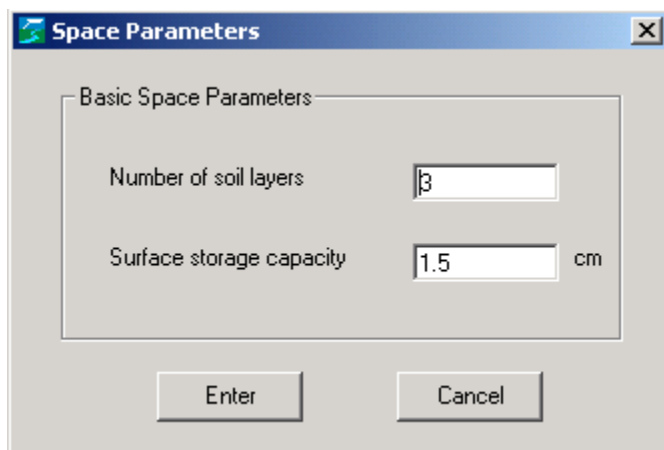
Number of soil layers: NL (In the current program,  $NL_{\max} = 50$ )

Number of cells for each soil layer: NC(I) (In the current program, the maximum number of the total soil cells is set as 1000)

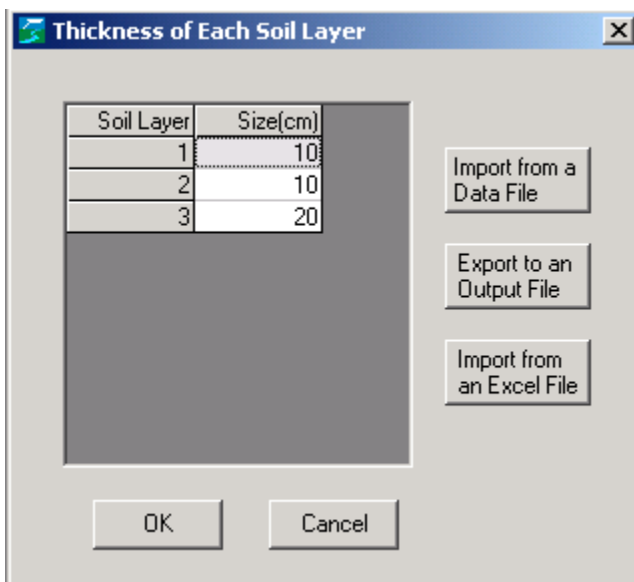
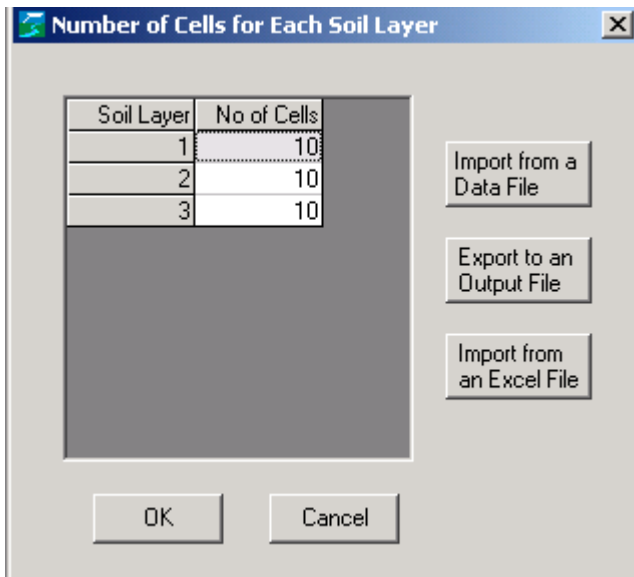
Thickness of each soil layer (cm): ZNL(I)

Surface storage capacity (cm): SSMAX

Based upon soil properties, the entire soil profile is divided into a number of soil layers. Each soil layer further consists of computation cells.



The screenshot shows a dialog box titled "Space Parameters". It contains two input fields: "Number of soil layers" with the value "3" and "Surface storage capacity" with the value "1.5" and the unit "cm". At the bottom, there are two buttons: "Enter" and "Cancel".

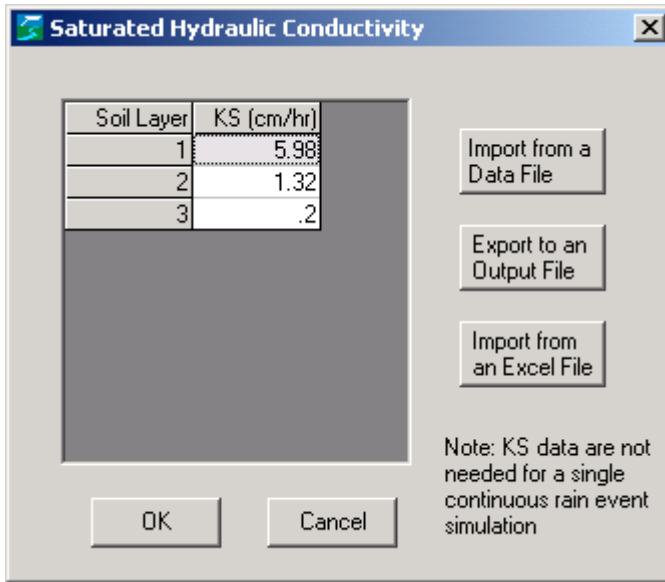


### 5.3 Soil Parameters

#### 5.3.1 Saturated Hydraulic Conductivity

Saturated Hydraulic Conductivity (cm/hr):  $K_S$

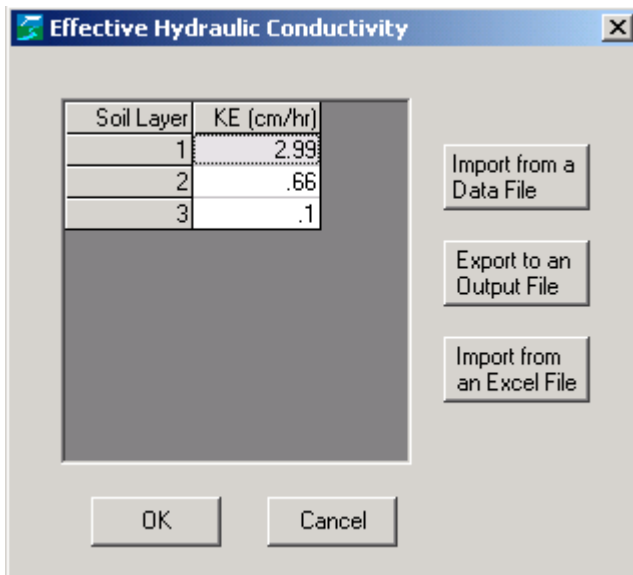
Input  $K_S$  value for each soil layer.  $K_S$  can be estimated using Table 1.



### 5.3.2 Effective Hydraulic Conductivity

Effective Hydraulic Conductivity (cm/hr): KE

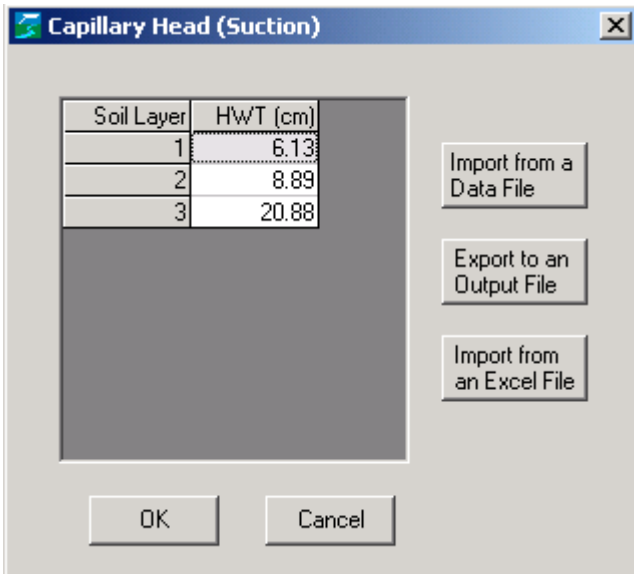
Input KE value for each soil layer. KE can be estimated from KS using Table 1.



### 5.3.3 Capillary Head (Suction)

Capillary Head (Suction) (cm): HWT

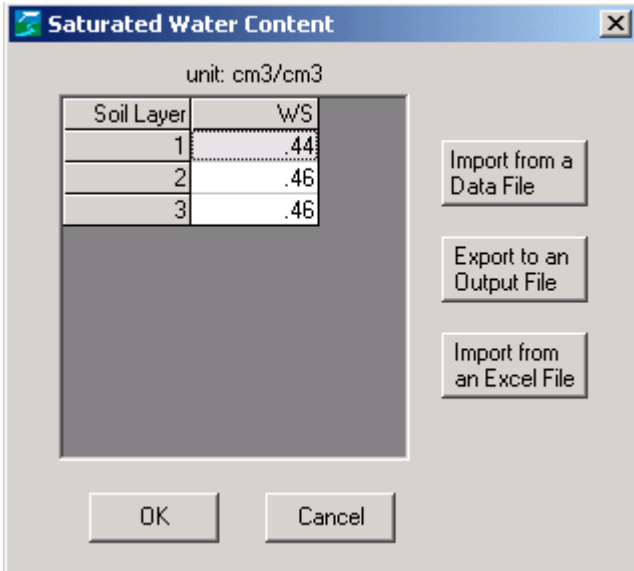
Input HWT value for each soil layer. HWT can be estimated using Table 2.



### 5.3.4 Saturated Water Content

Saturated Water Content ( $\text{cm}^3/\text{cm}^3$ ): WS

Input WS value for each soil layer. WS can be estimated using Table 3.

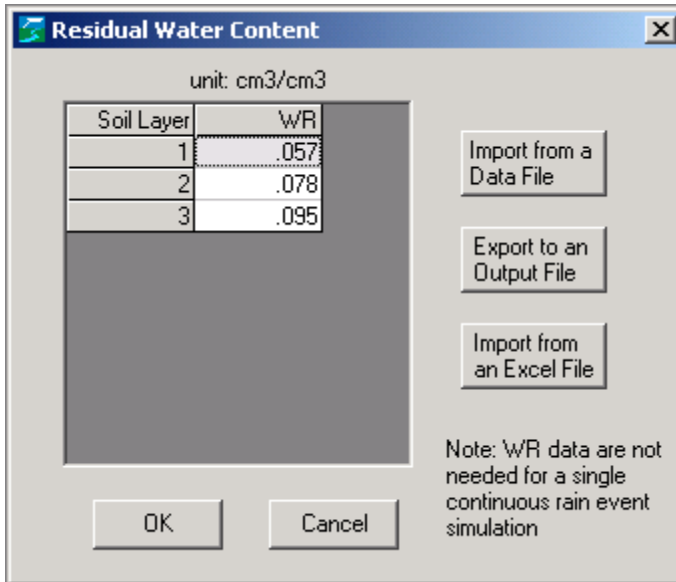


### 5.3.5 Residual Water Content

Residual Water Content ( $\text{cm}^3/\text{cm}^3$ ): WR

Input WR value for each soil layer. WR can be estimated using Table 4.

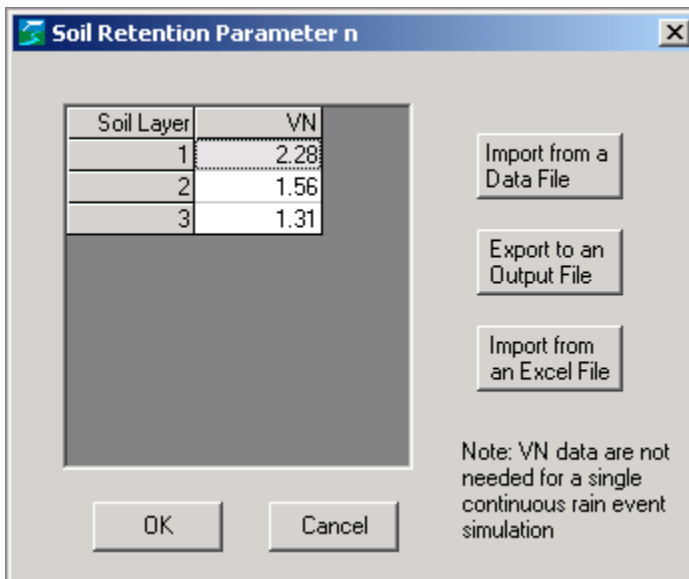




### 5.3.6 Soil Water Retention Parameter n

Soil Water Retention Parameter n: VN

“n” is a soil water retention parameter in the van Genuchten model. Input VN values for both surface/root zone and deep vadose zone. VN can be estimated by using Table 5.



### 5.3.7 Soil Water Retention Parameter $\alpha$

Soil Water Retention Parameter  $\alpha$  (1/cm): ALF

“ $\alpha$ ” is a soil water retention parameter in the van Genuchten model. Input ALF value for each soil layer. ALF can be estimated using Table 6.

Soil Layer	ALF(1/cm)
1	.124
2	.036
3	.019

### 5.3.8 Field Capacity

Field Capacity ( $\text{cm}^3/\text{cm}^3$ ): FC

Input FC value for each soil layer. FC can be estimated using Table 7. FC can also be estimated by using Figure 1 (Source: Carsel et al. 2003)

Soil Layer	FC
1	.1
2	.29
3	.32

### 5.3.9 Wilting Point

Wilting Point ( $\text{cm}^3/\text{cm}^3$ ): WP

Input WP values for each soil layer. WP can be estimated by using Table 8. WP can also be estimated by using Figure 2 (Source: Carsel et al. 2003).

Soil Layer	WP
1	.03
2	.05
3	.085

unit:  $\text{cm}^3/\text{cm}^3$

Note: WP data are not needed for a single continuous rain event simulation

### 5.3.10 Initial Water Content

Initial Water Content ( $\text{cm}^3/\text{cm}^3$ ): W0

Initial water content represents the average soil moisture condition in each discretized soil cell at the initial simulation time ( $t = 0$ ).

Input W0 values for each soil cell.

Soil Cell	W0
1	.1
2	.1
3	.1
4	.1
5	.1
6	.1
7	.1
8	.1
9	.1
10	.1

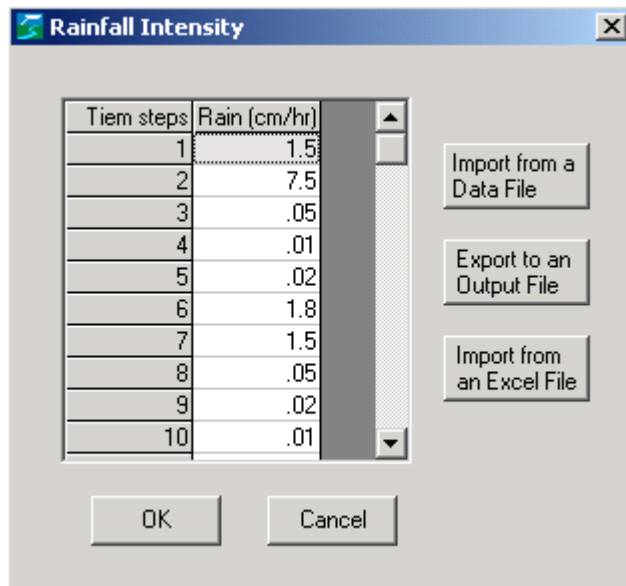
unit:  $\text{cm}^3/\text{cm}^3$

## 5.4 Meteorologic Data

### 5.4.1 Rainfall Intensity

Rainfall Intensity (cm/hr): RAINS

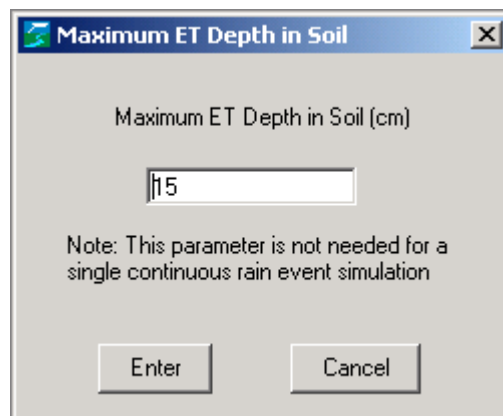
Rainfall intensity data are needed in the model. The data can be obtained from government agencies' climate centers, such as NOAA National Climatic Data Center (NCDC) and USDA-NRCS National Water and Climate Center (PRISM). Links to these websites can be found in menu Parameter Estimation.



### 5.4.2 Maximum ET Depth in Soil

Maximum ET Depth in Soil (cm): DMET

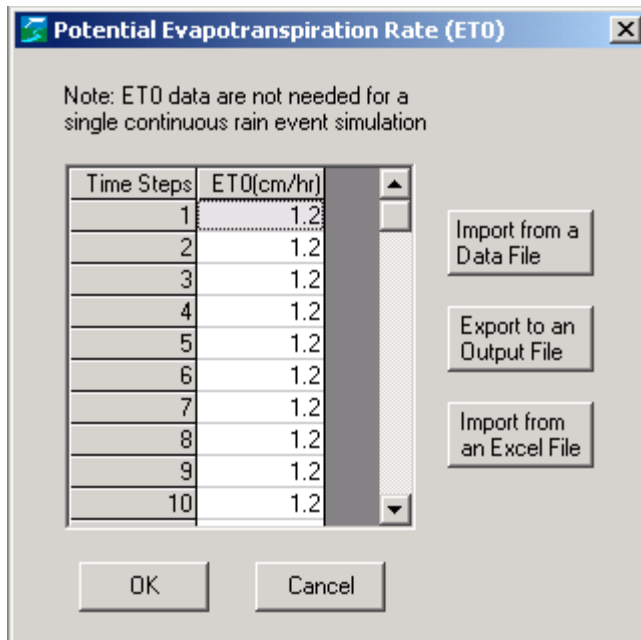
The maximum ET depth in soil is generally equal to the maximum depth of the crop root zone. The value depends on crop types.



### 5.4.3 Potential Evapotranspiration Rate

Potential Evapotranspiration Rate (cm/hr): ET<sub>0</sub>

Potential evapotranspiration rate data are needed in the model. The data can be obtained from government agencies' climate centers, such as NOAA National Climatic Data Center (NCDC) and USDA-NRCS National Water and Climate Center (PRISM). Links to these websites can be found in menu Parameter Estimation.



### 5.4.4. Crop Coefficient

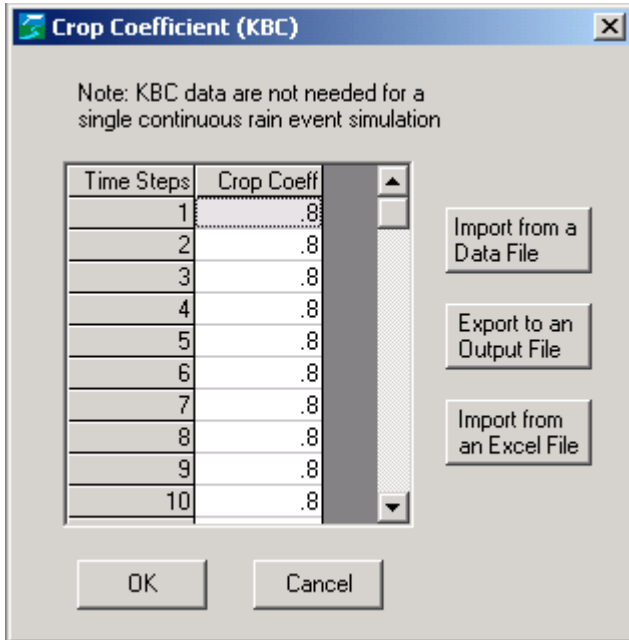
Crop Coefficient: KBC

Crop coefficient is the ratio of actual crop evapotranspiration ET<sub>c</sub> to the standard reference crop evapotranspiration (potential evapotranspiration) ET<sub>0</sub>.

$$KBC = ET_c/ET_0$$

The value of KBC can change with crop types and stages of crop growth. The KBC value is small during the initial crop stage, often less than 0.4. The value increases with rapid plant development and reaches a maximum value at the time of maximum or near maximum plant development (it generally ranges from 1.0 to 1.2). As leaves begin to age during the late period, the value begins to decrease until it reaches a lower value at the end of the growing period (Allen et al., 1998). The FAO Paper 56 (Allen et al., 1998) provides details on how to determine the crop coefficient. Users can access this reference via the menu Plant Websites. Single (time-averaged) crop

coefficients for three typical stages of crop growth (initial, mid, and end) and mean maximum plant heights for non stressed, well-managed crops in subhumid climates (RH<sub>min</sub> ≈ 45%, u<sub>2</sub> ≈ 2 m/s) can be found from Table 9 (Note: following the original notation, Kc denotes crop coefficient in this table).



## 5.5 Watershed Data

Watershed area (ha): AHA

Percentage of directly-connected impervious area (%): IMP

Time of concentration (hr): TC

Index of the unit hydrograph (1: SCS UH; 2: Clark UH): IUH

Basin storage coefficient in the Clark UH (hr): RC

Initial baseflow (m<sup>3</sup>/s): QB0

Baseflow recession constant: RB

Baseflow threshold value (ratio to the peak): RTHRE

Note that RC is required for the Clark unit hydrograph method only.

For watershed modeling, two unit hydrograph techniques (SCS UH and Clark UH) are available for selection. Baseflow is simulated by using the recession method as follows:

$$Q_B = Q_{B0} r_B^t$$

where  $Q_{B0}$  = initial baseflow;  $r_B$  = daily recession constant; and  $t$  = time (hr). Baseflow is constant ( $Q_{B0}$ ) for  $r_B = 1$ . Note that the recession constant is dependent on the unit of time (Maidment 1993, page 9.5). A daily recession constant is used in this program.

**Watershed Parameters** [X]

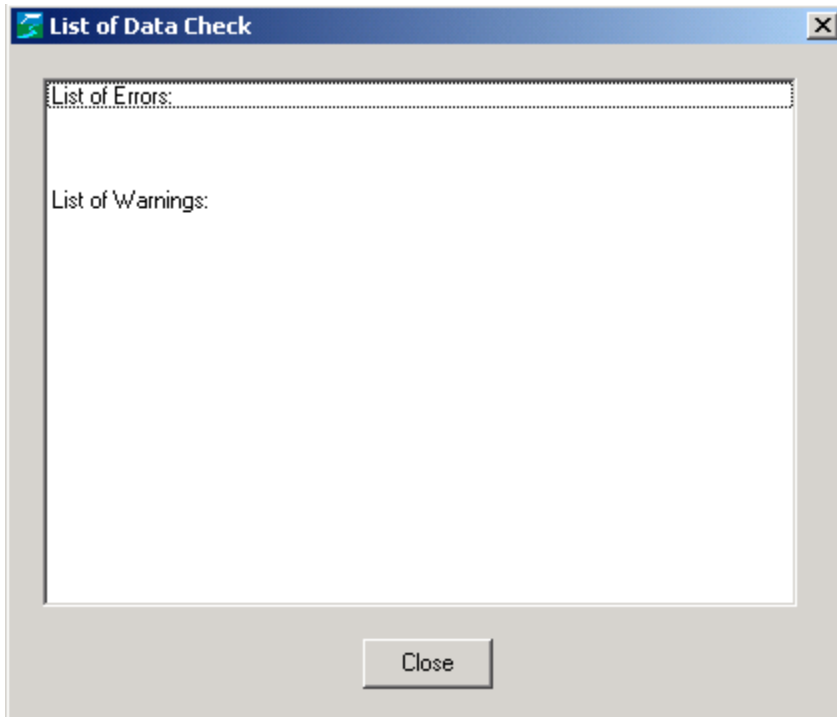
Watershed Hydrologic Modeling Parameters

Watershed Area (ha)	<input type="text" value="100"/>
Percent of Directly-Connected Impervious Area (%)	<input type="text" value="1"/>
Time of Concentration (hr)	<input type="text" value="5"/>
Index of the Unit Hydrograph (1: SCS UH; 2: Clark UH)	<input type="text" value="2"/>
Basin Storage Coefficient (hr) (for Clark UH only)	<input type="text" value="0.6"/>
Initial Baseflow (m <sup>3</sup> /s)	<input type="text" value="0.2"/>
Baseflow Recession Constant	<input type="text" value="0.9"/>
Baseflow Threshold Value (Ratio to the Peak)	<input type="text" value="0.1"/>

## 6. Data Check and Model Execution

### 6.1 Data Check

To make sure that all input data and relationship of some interrelated data are in reasonable ranges, the data should be checked by menu Check Data or button Check Data in the toolbar before running the model. Then, a list of warnings and errors will be shown. It is advised that you run the model after eliminating all warnings and errors.

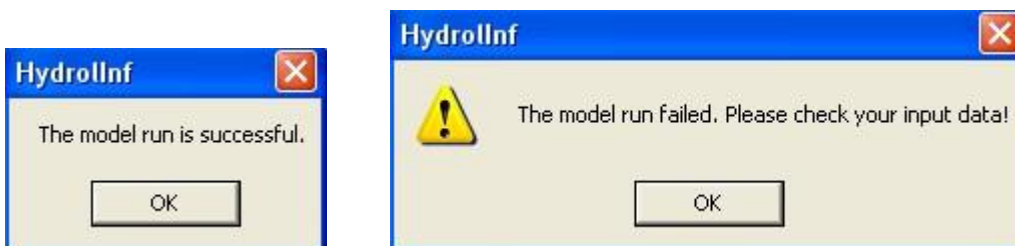


### 6.2 Model Run

Once all data are checked, the model can be executed by clicking Model-Run or button Run Model in the toolbar.

### 6.3 Check Model Run

Check whether or not the model run is successful.





## 7. Output and Post-Processing

### 7.1 Water Mass Balance Table and Graph

Water Mass Balance Table (button Output Table in the toolbar)

Rainfall/Infiltration/Runoff Graph (button Output Graphs in the toolbar)

Water Mass Balance Excel (button Transfer Output to Excel in the toolbar)

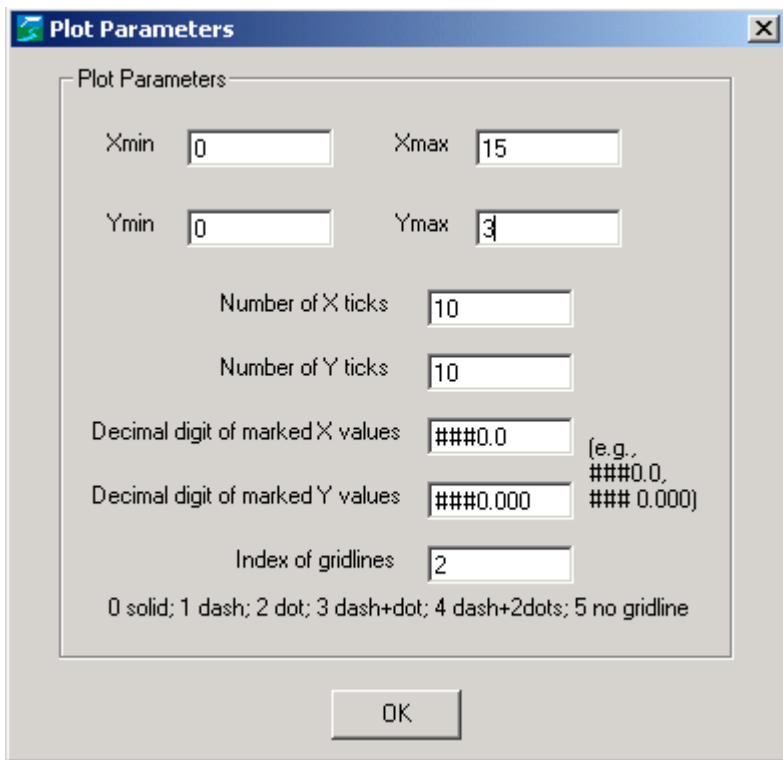
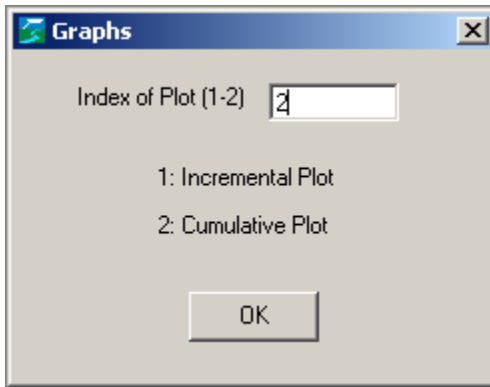
A water mass balance table shows incremental and cumulative rainfall (Rain, C-Rain), infiltration (Infil, C-Infil), runoff (Runf, C-Runf), and evapotranspiration from the surface water storage (ETS, C-ETS), as well as surface storage (SSTG) and the change in surface storage (D-Stg) for each time step.

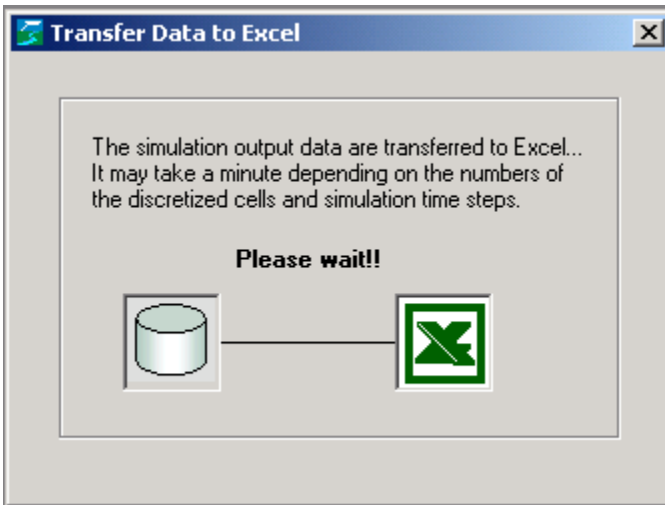
Both incremental and cumulative rainfall and the simulated infiltration and runoff can also be shown in form of graphs. A set of plot parameters will be automatically determined, which include minimum and maximum x values (time), minimum and maximum y values, number of x ticks, number of y ticks, decimal digit of marked x values, decimal digit of marked y values, index of gridlines (0 solid; 1 dash; 2 dot; 3 dash + dot; 4 dash + two dots; and 5 no gridline).

The simulated outputs can also be transferred to Microsoft Excel via menu Water Mass Balance Excel or button Transfer Output to Excel in the toolbar. Then these data can be analyzed by using Excel spreadsheet and graphs can also be created within Excel. Note that the data transfer may take a long time for a large data set.

Note that the mass balance terms in the aforementioned table and graph (e.g., runoff) are the depths of water over the pervious soil area only. For watershed modeling, total depth of runoff should include the quantities from both pervious area  $[(1-IMP/100)A]$  and directly-connected impervious area  $[IMP/100*A]$ .

Step	Time(hr)	Rain(cm)	Infil(cm)	Runf(cm)	ETS(cm)	D-Stg(cm)	P-I-R-E(cm)	C-Rain(cm)	C-Infil(cm)	C-Runf(cm)	C-ETS(cm)	SSTG(cm)
1	0.500	0.7500	0.7500	0.0000	0.0000	0.0000	0.0000	0.7500	0.7500	0.0000	0.0000	0.0000
2	1.000	3.7500	2.9331	0.0000	0.0000	0.8169	0.8169	4.5000	3.6831	0.0000	0.0000	0.8169
3	1.500	0.0250	0.8419	0.0000	0.0000	-0.8169	-0.8169	4.5250	4.5250	0.0000	0.0000	0.0000
4	2.000	0.0050	0.0050	0.0000	0.0000	0.0000	0.0000	4.5300	4.5300	0.0000	0.0000	0.0000
5	2.500	0.0100	0.0100	0.0000	0.0000	0.0000	0.0000	4.5400	4.5400	0.0000	0.0000	0.0000
6	3.000	0.9000	0.8987	0.0000	0.0000	0.0013	0.0013	5.4400	5.4387	0.0000	0.0000	0.0013
7	3.500	0.7500	0.7513	0.0000	0.0000	-0.0013	-0.0013	6.1900	6.1900	0.0000	0.0000	0.0000
8	4.000	0.0250	0.0250	0.0000	0.0000	0.0000	0.0000	6.2150	6.2150	0.0000	0.0000	0.0000
9	4.500	0.0100	0.0100	0.0000	0.0000	0.0000	0.0000	6.2250	6.2250	0.0000	0.0000	0.0000
10	5.000	0.0050	0.0050	0.0000	0.0000	0.0000	0.0000	6.2300	6.2300	0.0000	0.0000	0.0000
11	5.500	2.7500	0.5626	0.6874	0.0000	1.5000	1.5000	8.9800	6.7926	0.6874	0.0000	1.5000
12	6.000	0.0050	0.3952	0.0000	0.0000	-0.3902	-0.3902	8.9850	7.1878	0.6874	0.0000	1.1098
13	6.500	0.0050	0.3270	0.0000	0.0000	-0.3220	-0.3220	8.9900	7.5148	0.6874	0.0000	0.7878
14	7.000	0.0050	0.2872	0.0000	0.0000	-0.2822	-0.2822	8.9950	7.8021	0.6874	0.0000	0.5055
15	7.500	0.0100	0.2603	0.0000	0.0000	-0.2503	-0.2503	9.0050	8.0624	0.6874	0.0000	0.2552
16	8.000	1.7500	0.2405	0.2647	0.0000	1.2448	1.2448	10.7550	8.3029	0.9521	0.0000	1.5000
17	8.500	0.0000	0.1000	0.0000	0.4800	-0.5800	-0.5800	10.7550	8.4029	0.9521	0.4800	0.9200
18	9.000	0.4000	0.2277	0.0000	0.0000	0.1723	0.1723	11.1550	8.6306	0.9521	0.4800	1.0923
19	9.500	0.0000	0.1000	0.0000	0.4800	-0.5800	-0.5800	11.1550	8.7306	0.9521	0.9600	0.5123
20	10.000	0.0000	0.0323	0.0000	0.4800	-0.5123	-0.5123	11.1550	8.7629	0.9521	1.4400	0.0000
21	10.500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	11.1550	8.7629	0.9521	1.4400	0.0000
22	11.000	0.7500	0.6767	0.0000	0.0000	0.0733	0.0733	11.9050	9.4396	0.9521	1.4400	0.0733
23	11.500	1.2500	0.1982	0.0000	0.0000	1.0518	1.0518	13.1550	9.6377	0.9521	1.4400	1.1251
24	12.000	1.5000	0.1860	0.9392	0.0000	0.3749	0.3749	14.6550	9.8237	1.8913	1.4400	1.5000
25	12.500	0.5000	0.1796	0.3204	0.0000	0.0000	0.0000	15.1550	10.0034	2.2116	1.4400	1.5000
26	13.000	0.5000	0.1740	0.3260	0.0000	0.0000	0.0000	15.6550	10.1774	2.5376	1.4400	1.5000





## 7.2 Water Table for the Surface Zone

### Water Table for the Surface Zone

A cumulative water mass balance table for the surface zone shows cumulative rainfall (C-Rain), infiltration (C-Infil), runoff (C-Runf), evapotranspiration from the surface water storage (C-ETS), and the surface storage (SSTG) for each time step. Note that the mass balance terms in the table (e.g., runoff) are the depths of water over the pervious soil area only.

MassB-Surf

----- Mass Balance Table for the Surface Zone of the Pervious Soil Area -----

Step	T (hr)	C-Rain (cm)	C-Infil (cm)	C-Runf (cm)	C-ETS (cm)	SSTG (cm)	P-I-R-E (cm)
1	.5000	.750000	.750000	.000000	.000000	.000000	.000000
2	1.0000	4.500000	3.683087	.000000	.000000	.816913	.816913
3	1.5000	4.525000	4.525000	.000000	.000000	.000000	.000000
4	2.0000	4.530000	4.530000	.000000	.000000	.000000	.000000
5	2.5000	4.540000	4.540000	.000000	.000000	.000000	.000000
6	3.0000	5.440000	5.438715	.000000	.000000	.001285	.001285
7	3.5000	6.190000	6.190000	.000000	.000000	.000000	.000000
8	4.0000	6.215000	6.215000	.000000	.000000	.000000	.000000
9	4.5000	6.225000	6.225000	.000000	.000000	.000000	.000000
10	5.0000	6.230000	6.230000	.000000	.000000	.000000	.000000
11	5.5000	8.980000	6.792608	.687392	.000000	1.500000	1.500000
12	6.0000	8.985000	7.187781	.687392	.000000	1.109826	1.109826
13	6.5000	8.990000	7.514826	.687392	.000000	.787781	.787781
14	7.0000	8.995000	7.802062	.687392	.000000	.505546	.505546
15	7.5000	9.005000	8.062367	.687392	.000000	.255240	.255240
16	8.0000	10.755000	8.302892	.952108	.000000	1.500000	1.500000
17	8.5000	10.755000	8.402892	.952108	.480000	.920000	.920000
18	9.0000	11.155000	8.630575	.952108	.480000	1.092316	1.092316
19	9.5000	11.155000	8.730575	.952108	.960000	.512316	.512316
20	10.0000	11.155000	8.762892	.952108	1.440000	.000000	.000000

### 7.3 Water Table for the Vadose Zone

#### Water Table for the Vadose Zone

A cumulative water mass balance table for the vadose zone shows cumulative infiltration (C-Infil), evapotranspiration from the soil profile (C-ET), discharge to the underlying groundwater (C-GW), and changes in the soil water storage (soil water content) (D-WC) for each time step. Note that the mass balance terms in the table are the depths of water over the pervious soil area only.

MassB-Soil

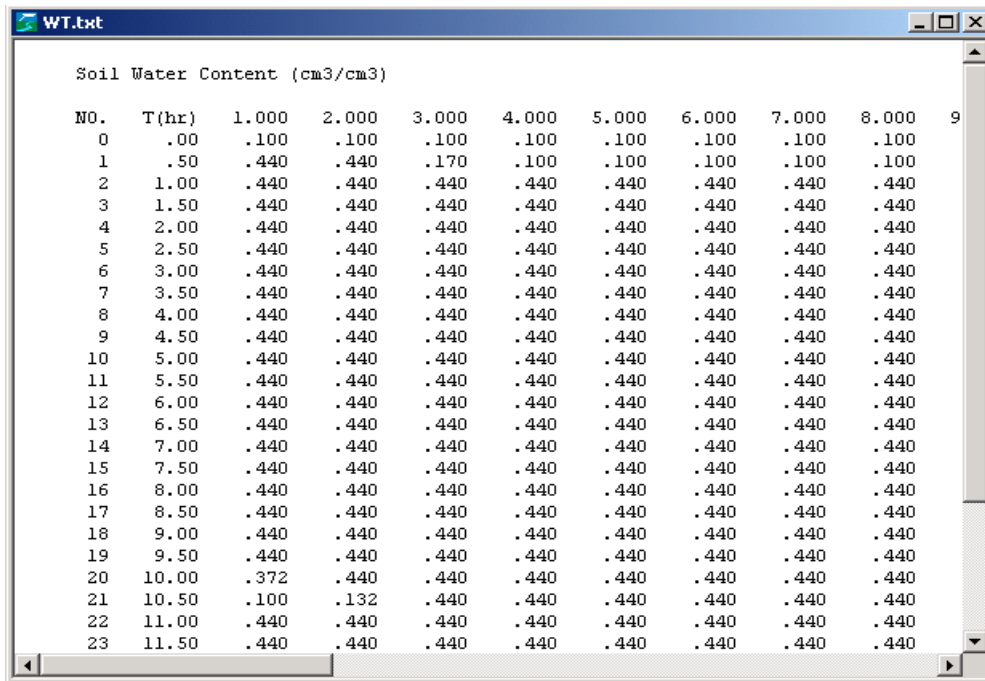
----- Mass Balance Table for the Vadose Zone under the Pervious Soil Area -----

Step	T (hr)	C-Infil (cm)	C-ET (cm)	C-GW (cm)	D-WC (cm)	I-ET-GW (cm)
1	.5000	.750000	.000000	.000000	.750000	.750000
2	1.0000	3.683087	.000000	.000000	3.683087	3.683087
3	1.5000	4.525000	.000000	.000000	4.525000	4.525000
4	2.0000	4.530000	.000000	.000000	4.530000	4.530000
5	2.5000	4.540000	.000000	.000000	4.540000	4.540000
6	3.0000	5.438715	.000000	.000000	5.438715	5.438715
7	3.5000	6.190000	.000000	.000000	6.190000	6.190000
8	4.0000	6.215000	.000000	.000000	6.215000	6.215000
9	4.5000	6.225000	.000000	.000000	6.225000	6.225000
10	5.0000	6.230000	.000000	.000000	6.230000	6.230000
11	5.5000	6.792608	.000000	.000000	6.792608	6.792608
12	6.0000	7.187781	.000000	.000000	7.187781	7.187781
13	6.5000	7.514826	.000000	.000000	7.514826	7.514826
14	7.0000	7.802062	.000000	.000000	7.802062	7.802062
15	7.5000	8.062367	.000000	.000000	8.062367	8.062367
16	8.0000	8.302892	.000000	.000000	8.302892	8.302892
17	8.5000	8.402892	.000000	.000000	8.402892	8.402892
18	9.0000	8.630575	.000000	.000000	8.630575	8.630575
19	9.5000	8.730575	.000000	.000000	8.730575	8.730575

## 7.4 Soil Water Content

### Soil Water Content

The soil water content table shows both temporal and spatial variations of soil moisture conditions.



Soil Water Content (cm3/cm3)										
NO.	T(hr)	1.000	2.000	3.000	4.000	5.000	6.000	7.000	8.000	9
0	.00	.100	.100	.100	.100	.100	.100	.100	.100	.100
1	.50	.440	.440	.170	.100	.100	.100	.100	.100	.100
2	1.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
3	1.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
4	2.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
5	2.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
6	3.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
7	3.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
8	4.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
9	4.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
10	5.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
11	5.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
12	6.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
13	6.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
14	7.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
15	7.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
16	8.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
17	8.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
18	9.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
19	9.50	.440	.440	.440	.440	.440	.440	.440	.440	.440
20	10.00	.372	.440	.440	.440	.440	.440	.440	.440	.440
21	10.50	.100	.132	.440	.440	.440	.440	.440	.440	.440
22	11.00	.440	.440	.440	.440	.440	.440	.440	.440	.440
23	11.50	.440	.440	.440	.440	.440	.440	.440	.440	.440

## 7.5 Soil Water Flow Velocity

### Soil Water Flow Velocity

The soil water flow velocity table shows both temporal and spatial variations of soil water flow velocities.

Soil Water Flow Velocity (cm/hr)									
NO.	T(hr)	.000	1.000	2.000	3.000	4.000	5.000	6.000	7.000
1	.50	1.500	.820	.140	.000	.000	.000	.000	.000
2	1.00	5.866	5.866	5.866	5.326	4.646	3.966	3.286	2.606
3	1.50	1.684	1.684	1.684	1.684	1.684	1.684	1.684	1.684
4	2.00	.010	.010	.010	.010	.010	.010	.010	.010
5	2.50	.020	.020	.020	.020	.020	.020	.020	.020
6	3.00	1.797	1.797	1.797	1.797	1.797	1.797	1.797	1.797
7	3.50	1.503	1.503	1.503	1.503	1.503	1.503	1.503	1.503
8	4.00	.050	.050	.050	.050	.050	.050	.050	.050
9	4.50	.020	.020	.020	.020	.020	.020	.020	.020
10	5.00	.010	.010	.010	.010	.010	.010	.010	.010
11	5.50	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125
12	6.00	.790	.790	.790	.790	.790	.790	.790	.790
13	6.50	.654	.654	.654	.654	.654	.654	.654	.654
14	7.00	.574	.574	.574	.574	.574	.574	.574	.574
15	7.50	.521	.521	.521	.521	.521	.521	.521	.521
16	8.00	.481	.481	.481	.481	.481	.481	.481	.481
17	8.50	.200	2.040	2.720	3.400	4.080	4.760	5.440	5.980
18	9.00	.455	.455	.455	.455	.455	.455	.455	.455
19	9.50	.200	1.225	1.905	2.585	3.265	3.945	4.625	5.305
20	10.00	.065	.200	.745	1.425	2.105	2.785	3.465	4.145
21	10.50	.000	.077	.453	.395	1.011	1.659	2.322	2.994
22	11.00	1.353	.673	.058	.058	.058	.058	.058	.058
23	11.50	.396	.396	.396	.396	.396	.396	.396	.396

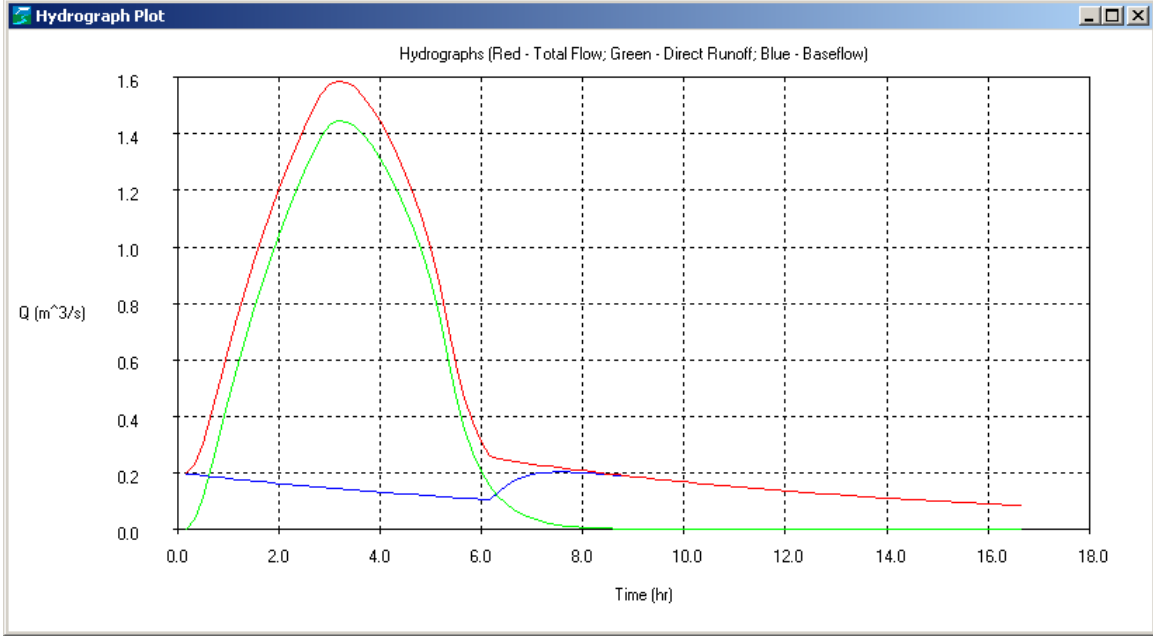
### 7.6 Flow Table for the Watershed Outlet

Mass balance table for the entire watershed. Note that the infiltration and runoff from the pervious and directly-connected impervious areas are the depths of water over the entire watershed area.

----- Water Table for the Entire Watershed -----								
Step	Time (hr)	Rain (cm)	Infl (cm)	Runoff-P (cm)	Runoff-IMP (cm)	Direct-Q (m3/s)	Baseflow (m3/s)	Total-Q (m3/s)
1	.50000	.750000	.749250	.000000	.000750	.000466	.189737	.190203
2	1.00000	3.750000	2.930154	.000000	.003750	.003630	.180000	.183630
3	1.50000	.025000	.841071	.000000	.000025	.007807	.170763	.178570
4	2.00000	.005000	.004995	.000000	.000005	.007170	.162000	.169170
5	2.50000	.010000	.009990	.000000	.000010	.003581	.153687	.157267
6	3.00000	.900000	.897816	.000000	.000900	.002057	.145800	.147857
7	3.50000	.750000	.750534	.000000	.000750	.002653	.138318	.140971
8	4.00000	.025000	.024975	.000000	.000025	.003129	.131220	.134349
9	4.50000	.010000	.009990	.000000	.000010	.002232	.124486	.126718
10	5.00000	.005000	.004995	.000000	.000005	.001080	.118098	.119178
11	5.50000	2.750000	.562045	.686705	.002750	.428902	.112038	.540940
12	6.00000	.005000	.394779	.000000	.000005	1.194788	.106288	1.301076
13	6.50000	.005000	.326718	.000000	.000005	1.190105	.100834	1.290939
14	7.00000	.005000	.286949	.000000	.000005	.598445	.095659	.694105
15	7.50000	.010000	.260045	.000000	.000010	.246438	.090750	.337189
16	8.00000	1.750000	.240284	.264451	.001750	.266916	.086093	.353009
17	8.50000	.000000	.099900	.000000	.000000	.503037	.081675	.584713
18	9.00000	.400000	.227456	.000000	.000400	.476931	.077484	.554415
19	9.50000	.000000	.099900	.000000	.000000	.238823	.073508	.312330
20	10.00000	.000000	.032284	.000000	.000000	.098744	.069736	.168479
21	10.50000	.000000	.000000	.000000	.000000	.040722	.075739	.116461

### 7.7 Hydrograph at the Watershed Outlet

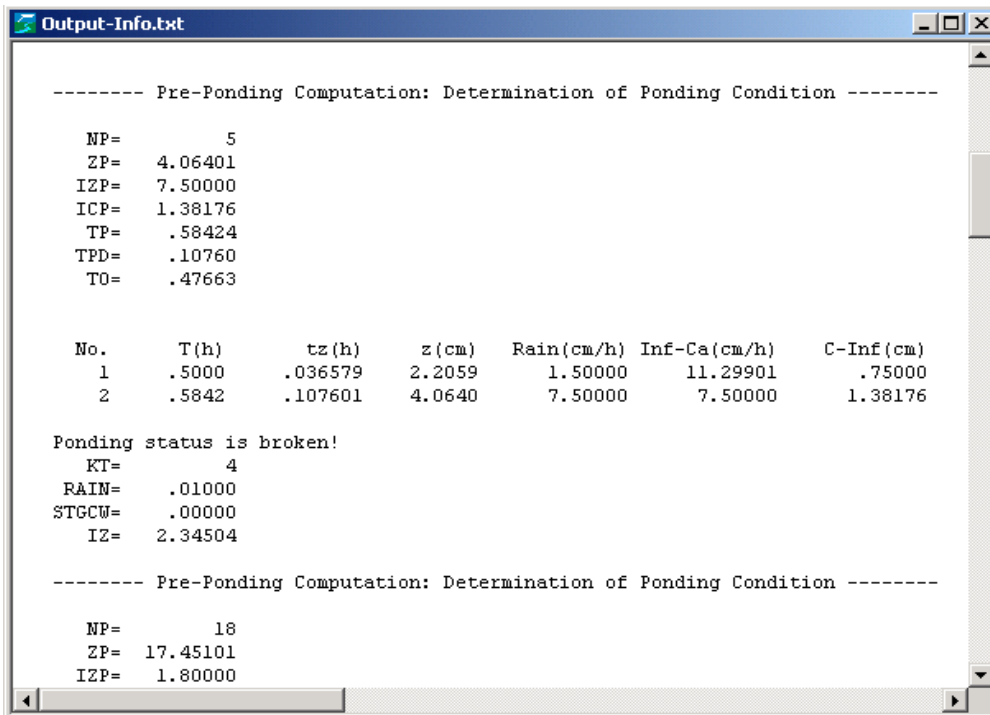
Hydrograph at the outlet



## 7.8 Model Output Information

### Model Output Information

It shows all input data, computation details of the model execution, such as determination of ponding condition.



## 8. SCS-CN Model

### 8.1 Theory of the Curve Number Method

The SCS-CN model is a separate model, in which the SCS-CN method is used to simulate surface runoff. The relevant theoretical information can be accessed via the menu of Theory of the CN Method, including equations, CN tables, P-Q curves, CN values for AMC-I, AMC-II, and AMC-III, and composite curve numbers with impervious areas. Note that the SCS-CN model should be used for event rainfall-runoff modeling only.

The screenshot shows a software window titled "Equations of the CN Method" with a close button in the top right corner. The window contains the following content:

Equations of the CN Method

$$Q = \frac{(P - I_a)^2}{(P - I_a) + S}$$
$$Q = \frac{(P - 0.2S)^2}{P + 0.8S}$$
$$Q = \frac{(P - 200/CN + 2)^2}{P + 800/CN - 8}$$

$I_a = 0.2S$        $S = \frac{1000}{CN} - 10$       For  $P > 0.2S$

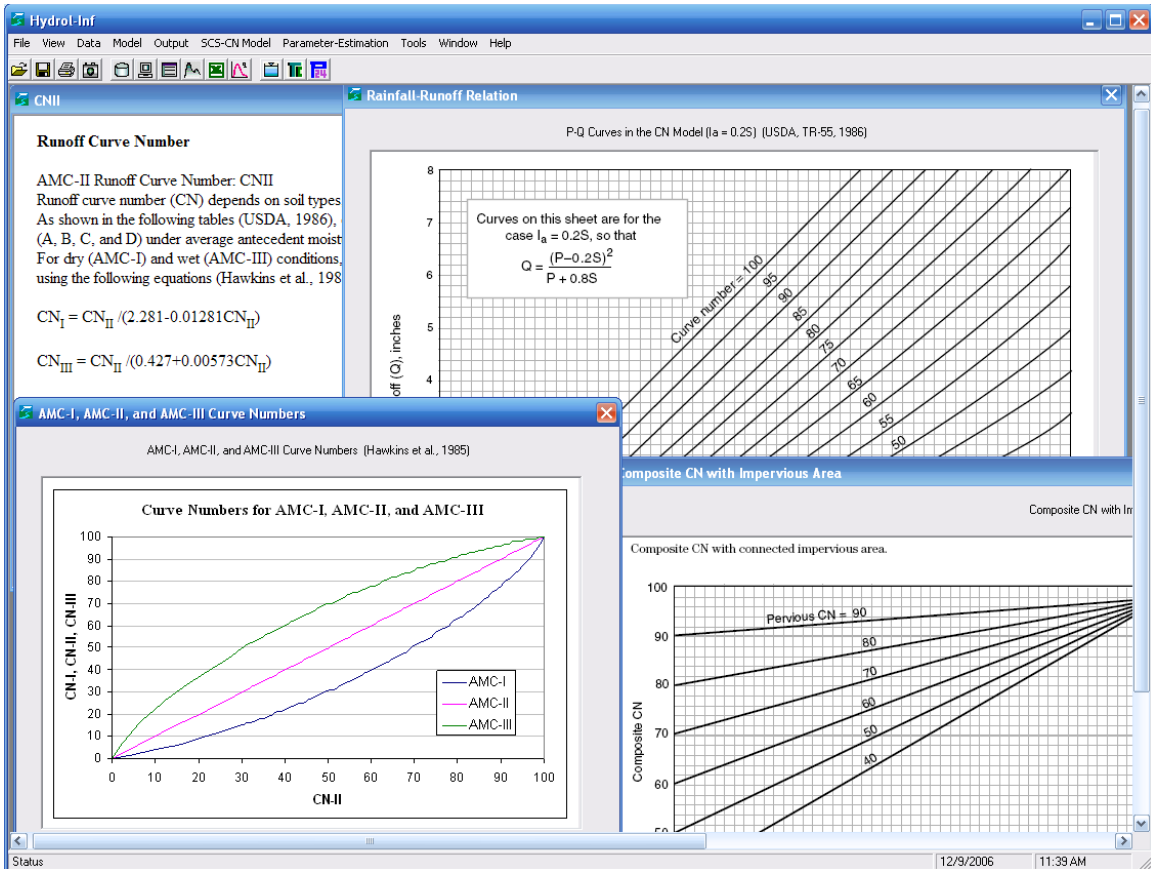
Notations

where Q = runoff (in); P = rainfall (in); S = potential maximum retention (in); and Ia = initial abstraction (in) (all initial losses: surface depression storage, vegetation interception, evaporation, and infiltration)

One parameter (CN), one input (P), one output (Q) model

Close

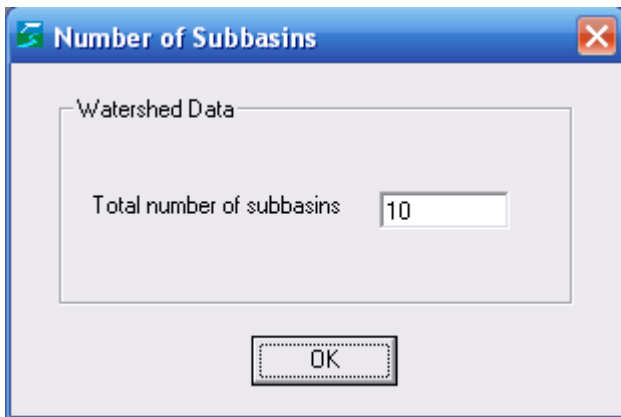
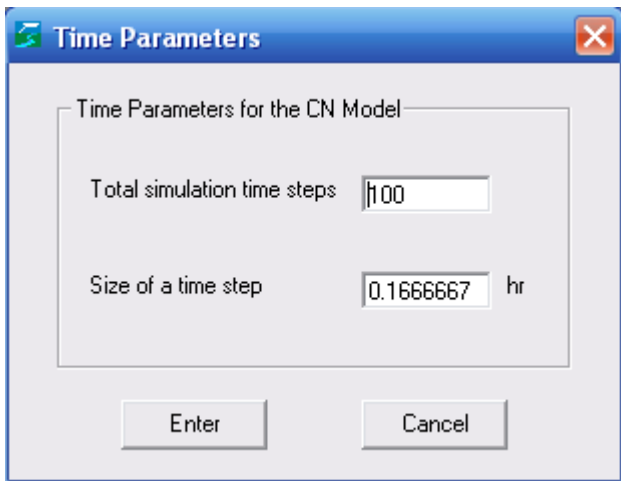
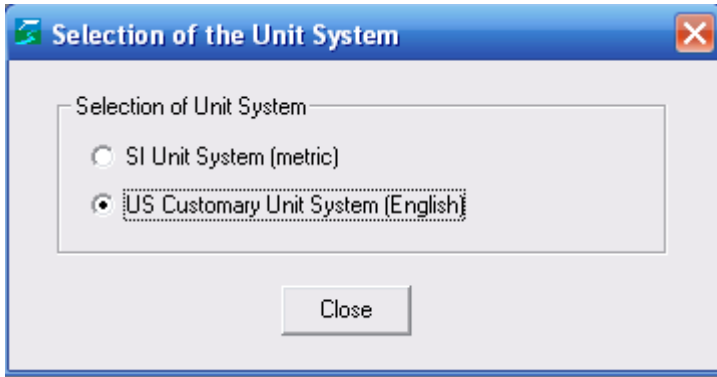




## 8.2 CN Rainfall-Runoff Modeling

In the CN rainfall-runoff modeling, two different unit systems (SI system and US customary unit system) can be selected. All modeling steps, including data preparation (import data, change working directory, input data, save data), model run and check, and output (view simulation summary tables and hydrographs) can be accessed through the menu SCS-CN Model. The modeling can be conducted for a single watershed or multiple watersheds. Comparison between the simulated and observed hydrographs can also be performed via the menu Calibration.

For watershed modeling, either SCS unit hydrograph or Clark unit hydrograph can be selected. Baseflow is simulated by using the recession method (see pages 28-29 for details). Note that the recession constant is dependent on the unit of time (Maidment 1993, page 9.5). A daily recession constant is used in this program.



**Watershed Parameters**

Watershed Parameters for the CN Model (one basin only)

Watershed Area (ha or mi <sup>2</sup> )	<input type="text" value="0.3861"/>
Percent of Directly-Connected Impervious Area (%)	<input type="text" value="1"/>
Time of Concentration (hr)	<input type="text" value="2"/>
Index of the Unit Hydrograph (1: SCS UH; 2: Clark UH)	<input type="text" value="2"/>
Basin Storage Coefficient (hr) (for Clark UH only)	<input type="text" value="2.5"/>
Initial Baseflow (m <sup>3</sup> /s or cfs)	<input type="text" value="3.00175"/>
Baseflow Recession Constant	<input type="text" value="0.9"/>
Baseflow Threshold Value (Ratio to the Peak)	<input type="text" value="0.1"/>
Curve Number	<input type="text" value="75"/>
Initial Abstraction Coefficient (default value = 0.2)	<input type="text" value="0.2"/>

**Watershed Data - Subbasin Information**

Watershed Data - Parameters for all subbasins

Basin	IUH	AHA	IMP(%)	TC(hr)	RC(hr)	QB0	RB	RTHRE	CN	IAC
Basin 1	2	.3861	1	2	2.5	3.00175	.9	.1	75	.2
Basin 2	2	.1	2	.3	1	1	.95	.1	80	.2
Basin 3	2	.2	5	.4	1.1	1.1	.93	.1	75	.2
Basin 4	2	.4	3.2	.5	1.3	1.2	.92	.1	68	.2
Basin 5	2	.5	.5	.8	1.8	1.5	.92	.1	78	.2
Basin 6	2	1.2	3	2	2.5	2	.91	.1	75	.2
Basin 7	2	3.1	6	3.6	4.5	5.1	.95	.15	83	.2
Basin 8	2	1.3	4	2.5	2	3.1	.93	.1	65	.2
Basin 9	2	5.1	1.3	5	8.5	6.5	.94	.2	70	.2
Basin 10	2	.1	3.5	.2	.6	.5	.9	.1	55	.2

IUH = Index of Unit Hydrograph Method (1: SCS UH; 2: Clark UH)  
 AHA = Basin Area (ha or mi<sup>2</sup>)  
 IMP = Percent of Directly-Connected Impervious Area (%)  
 TC = Time of Concentration (hr)  
 RC = Basin Storage Coefficient (hr) (for Clark UH only)

QB0 = Initial Baseflow (m<sup>3</sup>/s or cfs)  
 RB = Baseflow Recession Constant  
 RTHRE = Baseflow Threshold Value (Ratio to the Peak)  
 CN = Curve Number  
 IAC = Initial Abstraction Coefficient (Default Value = 0.2)

OK Cancel

**Rainfall**

Time steps	Rain (in)
1	0.78740
2	1.37795
3	0.47244
4	0.31496
5	0.00000
6	0.00000
7	0.00000
8	0.00000
9	0.00000
10	0.00000
11	0.00000

Generate 24-hr Rainfall

Import from a Data File

Export to an Output File

Import from an Excel File

OK Cancel

**Reach Routing Parameter - Lag Time**

Stream Reach Routing Parameter - Lag Time (Tavel Time)  
 Basin-in: Basin that discharges to outlet of the reach  
 Outlet-in: Inlet of the reach

Reach	Basin-in No	Outlet-in No	Lag Time(hr)
Reach 1	2	1	.2
Reach 2	3	2	1.3
Reach 3	4	3	.5
Reach 4	5	4	.7
Reach 5	6	5	1.1
Reach 6	7	6	2.1
Reach 7	8	7	.9
Reach 8	9	8	3.8
Reach 9	10	9	.5

OK

Cancel

Connections of Basins, Outlets, and Reaches

----- Water Table for Subbasin: 1

Step	T(hr)	Rain(in)	Inf(in)	Runf(in)	C-Rain(in)	C-Inf(in)	C-Runf(in)	Q-Peak(cfs)	T-Peak(hr)
1	.1667	.787402	.783182	.004220	.787402	.783182	.004220	1.754959	1.283333
2	.3333	1.377950	.917342	.460608	2.165352	1.700524	.464828	68.407120	1.283333
3	.5000	.472441	.204803	.267638	2.637793	1.905326	.732467	39.270359	1.283333
4	.6667	.314961	.117404	.197557	2.952754	2.022730	.930024	28.938242	1.283333
5	.8333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
6	1.0000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
7	1.1667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
8	1.3333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
9	1.5000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
10	1.6667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
11	1.8333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
12	2.0000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
13	2.1667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
14	2.3333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
15	2.5000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
16	2.6667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
17	2.8333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
18	3.0000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
19	3.1667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
20	3.3333	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
21	3.5000	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000
22	3.6667	.000000	.000000	.000000	2.952754	2.022730	.930024	.000000	.000000

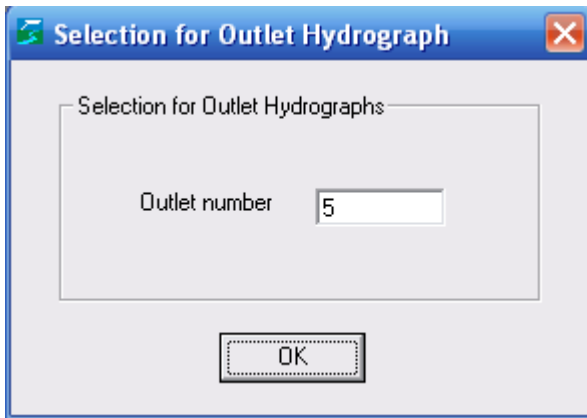
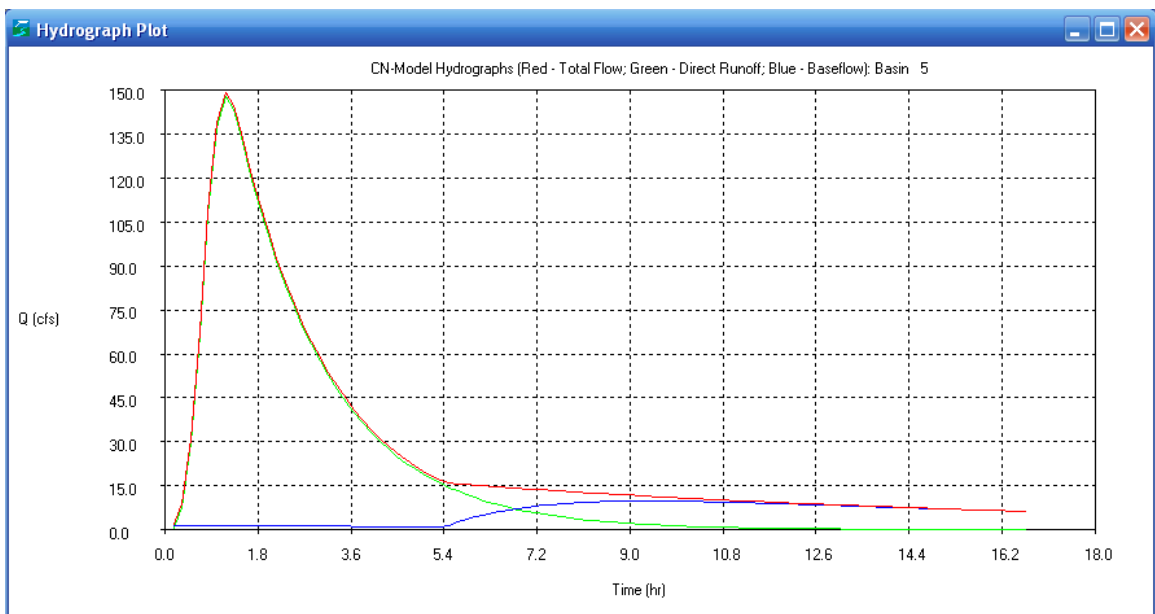
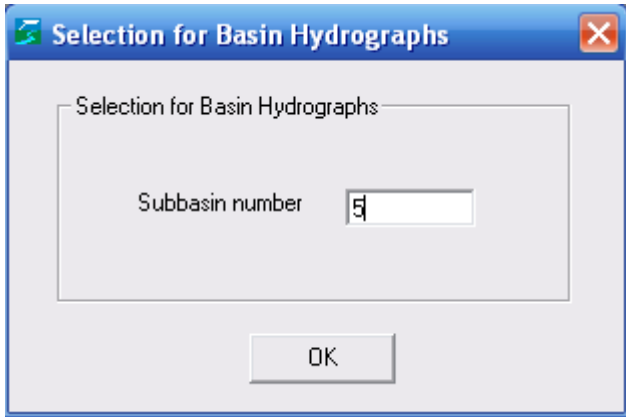
----- Flow Summary Table for Subbasin: 1

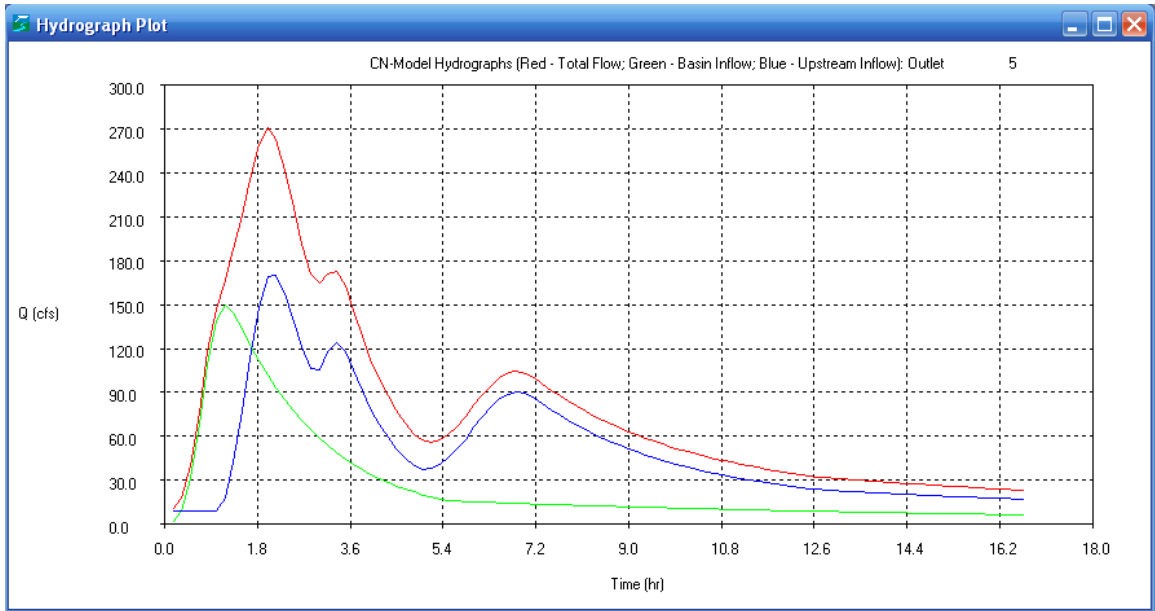
Peak Time (hour) = 2.16667  
Peak Flow (cfs) = 66.978622

Step	Time (hr)	Rain (in)	Runoff-P (in)	Runoff-IMP (in)	Direct-Q (cfs)	Baseflow (cfs)	Total-Q (cfs)
1	.16667	.787402	.004220	.007874	.019770	2.949499	2.969269
2	.33333	1.377950	.460608	.013779	.845045	2.898158	3.743203
3	.50000	.472441	.267638	.004724	3.495555	2.847710	6.343265
4	.66667	.314961	.197557	.003150	8.183248	2.798141	10.981389
5	.83333	.000000	.000000	.000000	14.537407	2.749434	17.286841
6	1.00000	.000000	.000000	.000000	21.999426	2.701575	24.701001
7	1.16667	.000000	.000000	.000000	30.216844	2.654549	32.871393
8	1.33333	.000000	.000000	.000000	38.738695	2.608342	41.347037
9	1.50000	.000000	.000000	.000000	46.816668	2.562939	49.379607
10	1.66667	.000000	.000000	.000000	53.767044	2.518326	56.285370
11	1.83333	.000000	.000000	.000000	59.197112	2.474490	61.671602
12	2.00000	.000000	.000000	.000000	62.906268	2.431417	65.337686
13	2.16667	.000000	.000000	.000000	64.589528	2.389094	66.978622
14	2.33333	.000000	.000000	.000000	63.812315	2.347508	66.159822
15	2.50000	.000000	.000000	.000000	61.059850	2.306645	63.366495
16	2.66667	.000000	.000000	.000000	57.446502	2.266494	59.712996
17	2.83333	.000000	.000000	.000000	53.740276	2.227041	55.967317

----- Flow at Outlet 1

Time (hr)	Q (cfs)
.16667	2.969269
.33333	3.743203
.50000	6.343265
.66667	10.981389
.83333	17.286841
1.00000	24.701001
1.16667	32.871393
1.33333	41.347037
1.50000	49.379607
1.66667	56.285370
1.83333	61.671602
2.00000	65.337686
2.16667	66.978622
2.33333	66.159822
2.50000	63.366495
2.66667	59.712996
2.83333	55.967317
3.00000	52.461436
3.16667	49.179915





Hydrograph Comparison

Observed Stream Flow Data

Hydrograph Selection

Select one type

Outlet hydrograph

Basin hydrograph

Outlet/subbasin number

6

Time steps	Qobs(cfs)
1	10
2	10
3	20
4	50
5	50
6	110
7	120
8	200
9	230
10	250

Import from a Data File

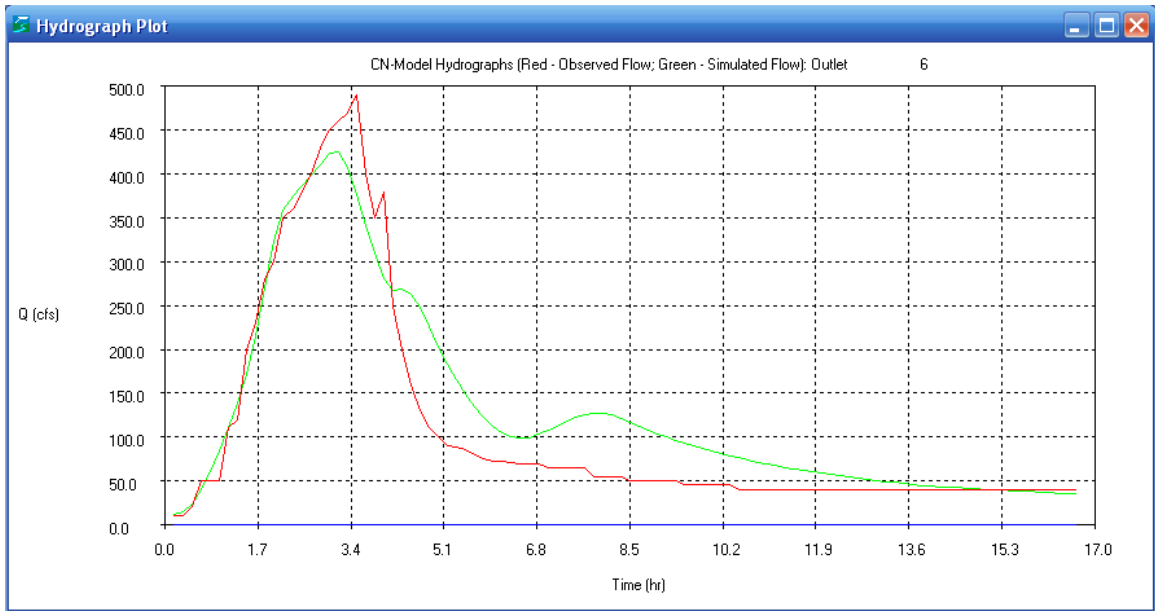
Export to an Output File

Import from an Excel File

Compare Simulated and Observed Hydrographs

Close

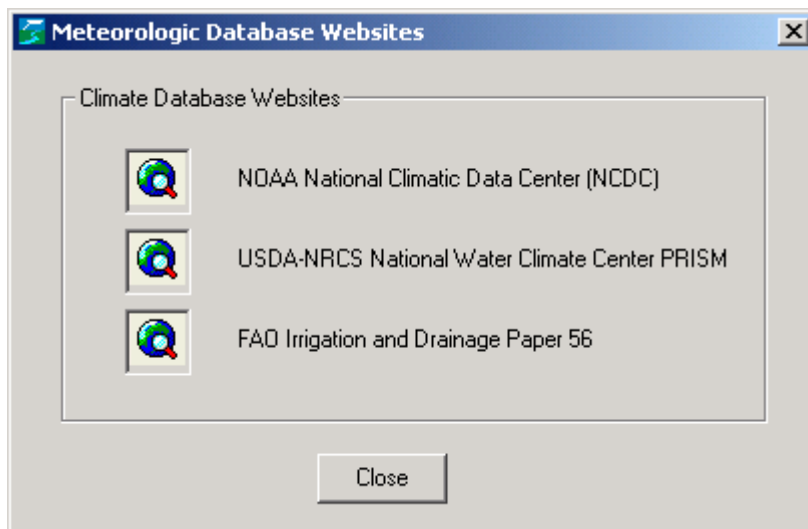
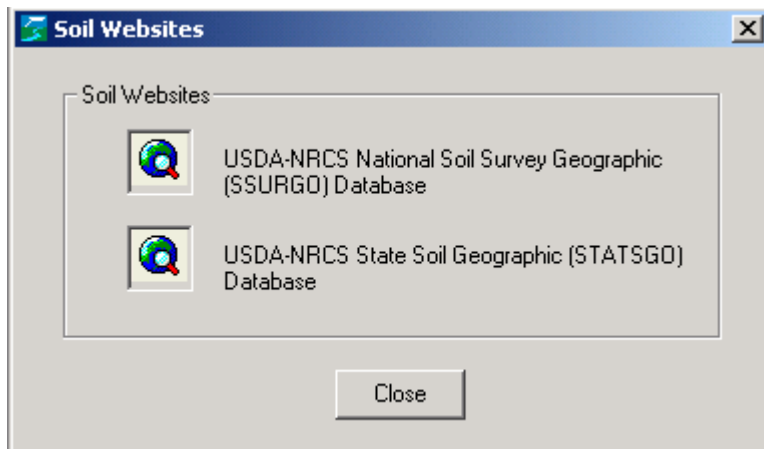




## 9. Introduction to the Data Supporting System: Parameter Estimation

To facilitate parameter estimation, a comprehensive data supporting system is developed and incorporated in Hydrol-Inf. All parameters/data used in the model are detailed in the data supporting system. It covers all basic data information, tables, and figures related to soil properties and meteorologic conditions that are included in this document.

The data supporting system also includes links to some useful database websites concerning soils and climate.



## 10. Hydrologic Tools

### 10.1 Computation of Measured Flow

#### Computation of Discharge

Generally, both velocity and depth of a stream change significantly over a cross-sectional area. The velocity near the water surface is greater than one close to the bottom and the water in the center of the stream flows faster than on the edges. Discharge of a stream through a cross-sectional area  $A$  can be expressed as:

$$Q = \iint_A V dA = \iint_A V(x, y) dx dy$$

in which  $Q$  = water discharge [ $L^3/T$ ];  $V$  = velocity [ $L/T$ ]; and  $A$  = area [ $L^2$ ].

A number of methods can be used for estimating discharge of a stream. Velocity-area methods are commonly used. Midsection method and mean-section method are two velocity-area methods and the former is generally recommended. As shown in the figure on the following page, the midsection method for calculating water discharge in a stream channel can be written as:

$$q_i = \bar{V}_i A_i = \bar{V}_i \left( \frac{L_{i+1} - L_i}{2} + \frac{L_i - L_{i-1}}{2} \right) d_i = \bar{V}_i \frac{L_{i+1} - L_{i-1}}{2} d_i \quad (i = 2, 3, \dots, n-1)$$

For the first and last sections, following equations are used for calculating the corresponding discharge (Gupta, 1989):

$$q_1 = \bar{V}_1 \frac{L_2 - L_1}{2} d_1$$

in which  $\bar{V}_1 = 0.65 \bar{V}_2$

$$q_n = \bar{V}_n \frac{L_n - L_{n-1}}{2} d_n$$

in which  $\bar{V}_n = 0.65 \bar{V}_{n-1}$

Hence, the total discharge can be given by:

$$Q = \sum_{i=1}^n q_i$$

in which  $q_i$  = water discharge of section  $i$  [ $L^3/T$ ];  $\bar{V}_i$  = mean velocity at observation point/vertical  $i$  [ $L/T$ ];  $L_i$  = distance from the initial point to observation point/vertical  $i$  [ $L$ ]; and  $d_i$  = depth of water at observation point/vertical  $i$  [ $L$ ].

The number of observation points/verticals or the size of each section depends on the entire width of the stream, variability in the stream depth and velocity, and the degree of precision required (research purposes). Usually, the number of sections/verticals

may range from 5 to 20. Some references suggest that 20-30 verticals of equidistant or variable spacings be used to divide a stream width. These spacings also should be arranged so that no section contains more than 10% of the total flow.

Computation of Mean Velocity:

- (1) One-Point Method (0.6D): A velocity is measured at a depth of 0.6D (D is the total depth of water) and it is assumed that this velocity is equal to the mean velocity as shown in the following equation. This method is suitable for  $D \leq 2ft$

$$\bar{V}_i = v_i^{0.6D}$$

- (2) Two-Point Method (0.2D & 0.8D): Two velocities are measured at depths of 0.2D and 0.8D. The mean velocity is estimated as follows. This method is suitable for  $D = 2 - 10ft$

$$\bar{V}_i = \frac{1}{2} v_i^{0.2D} + \frac{1}{2} v_i^{0.8D}$$

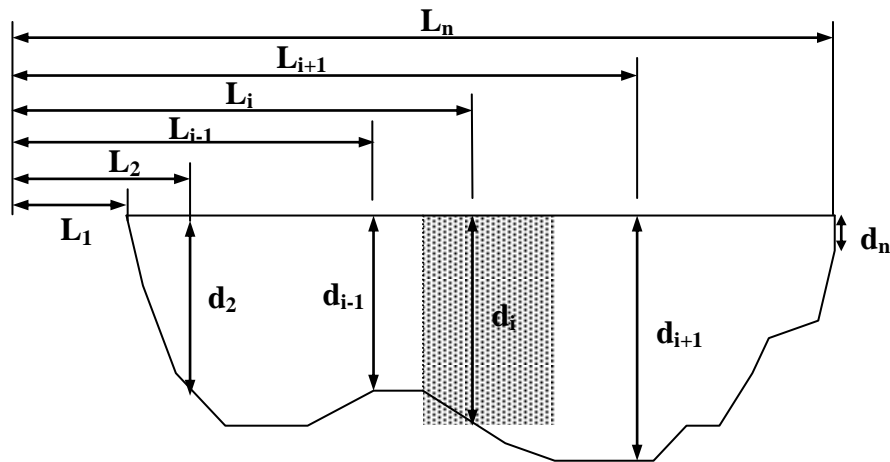
- (3) Three-Point Method (0.2D, 0.6D, & 0.8D): Three velocities are measured at depths of 0.2D, 0.6D, and 0.8D. The mean velocity is estimated as follows. This method is suitable for  $D = 10 - 20ft$

$$\bar{V}_i = \frac{1}{4} v_i^{0.2D} + \frac{1}{2} v_i^{0.6D} + \frac{1}{4} v_i^{0.8D}$$

- (4) 0.2-Depth Method (0.2D): In this method, it is assumed that the mean velocity equals 0.87 of the velocity measured at a depth of 0.2D.

$$\bar{V}_i = \alpha v_i^{0.2D} = 0.87 v_i^{0.2D}$$

The first two methods are widely used in practice.



Computation of Other Hydraulic Parameters:

(1) Overall Average Velocity:

$$\bar{V} = \frac{Q}{A} = \frac{\sum_{i=1}^n q_i}{\sum_{i=1}^n A_i}$$

(2) Wetted Perimeter:

$$WP = d_1 + \sum_{i=2}^n \sqrt{(d_i - d_{i-1})^2 + (L_i - L_{i-1})^2} + d_n$$

(3) Hydraulic Radius:

$$R = \frac{A}{WP}$$

(4) Conveyance Factor:

$$f_K = AR^{2/3}$$

(5) Slope-Roughness Factor:

$$f_{sr} = \frac{Q}{AR^{2/3}}$$

Computation of Measured Flow

Total number of measured points (N >= 3)

Selection of Unit System

SI Unit System (metric)

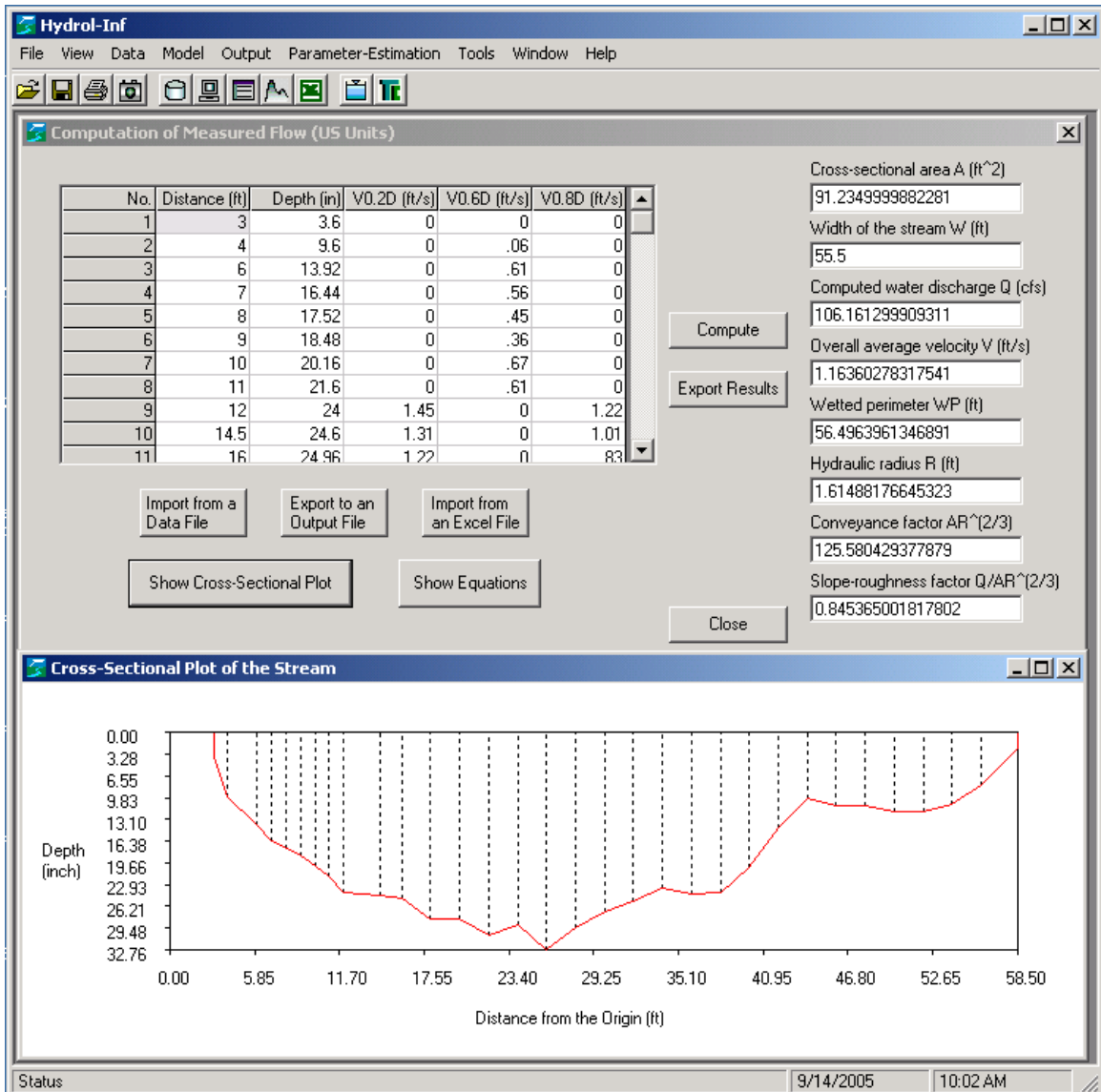
US Customary Unit System (English)

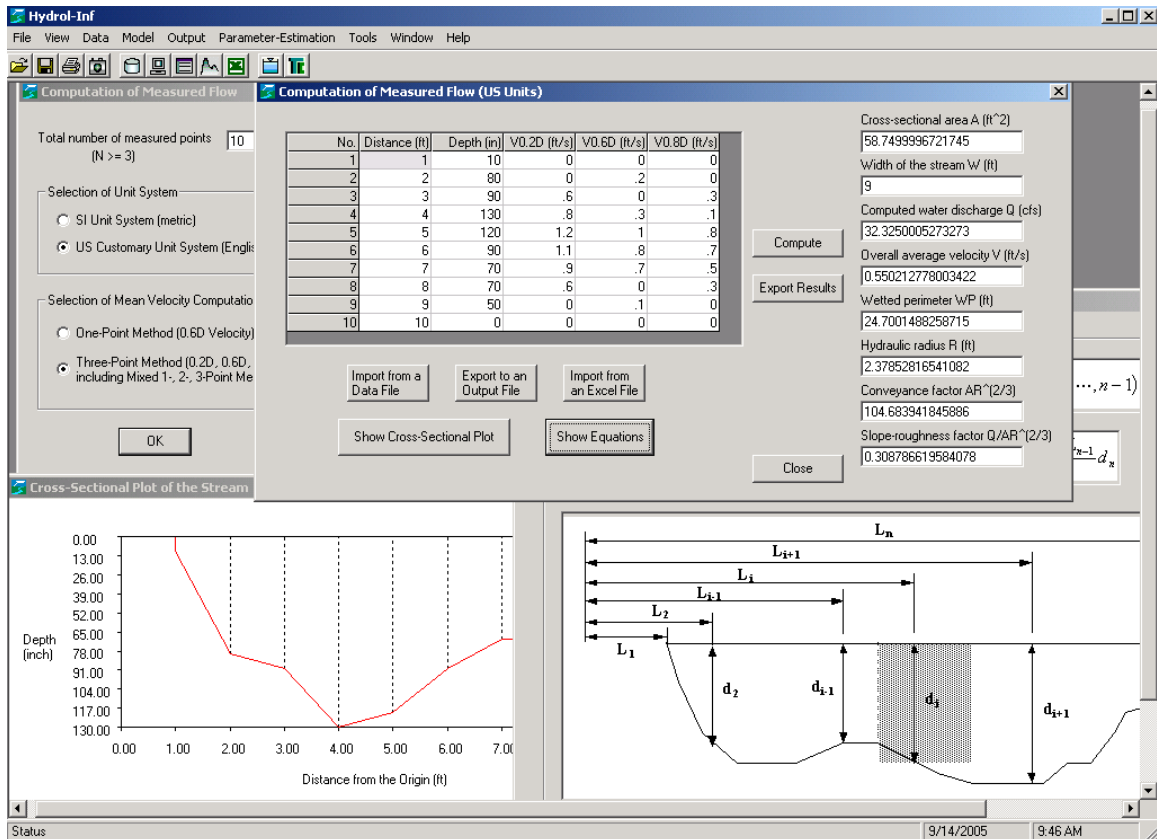
Selection of Mean Velocity Computation Methods

One-Point Method (0.6D Velocity)

Three-Point Method (0.2D, 0.6D, 0.8D Velocities), including Mixed 1-, 2-, 3-Point Methods

OK Cancel





## 10.2 Time of Concentration Calculator

Time of concentration can be estimated by using the following methods depending upon actual conditions (ASCE, 1996; USDA, 1986; Wanielista et al., 1997).

### 1) Kirpich

$$T_c = 0.0078 \frac{L^{0.77}}{S^{0.385}}$$

where  $L$  = length of flow (ft) and  $S$  = slope (ft/ft)

Application Conditions: small rural basins (1.2-112 acres); steep slopes (3%-10%); overland flow on bare soil; for overland flow on concrete or asphalt surfaces multiply by 0.4; for concrete channels multiply by 0.2.

### 2) Izzard

$$T_c = \frac{41.025(0.0007i + c_r)L^{1/3}}{S^{1/3}i^{2/3}}$$

where  $i$  = rainfall intensity (in/hr),  $c_r$  = retardation coefficient,  $L$  = length of flow (ft), and  $S$  = slope (ft/ft)

Application Conditions: overland flow on roadway and turf surface;  $iL < 500$  in. ft/hr; Requires iteration;  $c_r = 0.007$  for very smooth pavement (asphalt);  $c_r =$

0.0075 for tar and sand pavement;  $c_r = 0.012$  for concrete pavement;  $c_r = 0.06$  for dense turf.

3) Kerby

$$T_c = 0.8262 \frac{L^{0.467} n^{0.467}}{S^{0.2335}}$$

where  $n$  = Manning roughness coefficient or retardation coefficient,  $L$  = length of flow (ft), and  $S$  = mean slope of the basin (ft/ft).

Application Conditions: overland flow on small watersheds (<4.047 ha or 10 ac);  $L < 1000$  ft;  $n = 0.02$  for smooth pavement;  $n = 0.3$  for poor grass;  $n = 0.4$  for average grass;  $n = 0.8$  for dense grass.

4) Federal Aviation Agency

$$T_c = \frac{0.3884(1.1 - C)L^{0.5}}{S^{0.333}}$$

where  $C$  = rational runoff coefficient,  $L$  = length of overland flow (ft), and  $S$  = average overland slope (ft/ft).

Application Conditions: overland flow; frequently used for urban basins.

5) Kinematic Wave

$$T_c = \frac{0.93L^{0.6} n^{0.6}}{i^{0.4} S^{0.3}}$$

where  $n$  = Manning roughness coefficient for overland flow,  $L$  = length of overland flow (ft),  $i$  = rainfall intensity (in/hr), and  $S$  = average overland slope (ft/ft).

Application Conditions: overland flow;  $L < 300$  ft; requires iteration.

6) SCS Lag Equation

$$T_c = \frac{L^{0.8} \left( \frac{1000}{CN} - 9 \right)^{0.7}}{189.62S^{0.5}}$$

where  $L$  = watershed hydraulic length (ft),  $CN$  = runoff curve number, and  $S$  = average watershed slope (ft/ft).

Application Conditions: agricultural watersheds; small urban basins (< 2000 acres); assuming  $T_c = 1.67 T_L$ .

7) NRCS TR-55

Sheet flow travel time (min),  $T_{st}$

$$T_{st} = \frac{0.42(n_{st} L_{st})^{0.8}}{P_2^{0.5} S_{st}^{0.4}}$$

where  $n_{st}$  = Manning's roughness coefficient for sheet flow,  $L_{st}$  = sheet flow length (ft) ( $L_{st} \leq 300$  ft);  $P_2$  = 2-year, 24-hour rainfall (in), and  $S_{st}$  = slope of hydraulic grade line (land slope, ft/ft).

Shallow concentrated flow travel time (min),  $T_{sc}$



$$T_{sc} = \frac{L_{sc}}{60 C_c S_{sc}^{0.5}}$$

where  $L_{sc}$  = shallow concentrated flow length (ft),  $C_c$  = channel type coefficient (unpaved channel:  $C_c = 16.1345$ ; paved channel:  $C_c = 20.3282$ ), and  $S_{sc}$  = slope of hydraulic grade line (watercourse slope, ft/ft).

Open Channel flow travel time (min),  $T_{oc}$

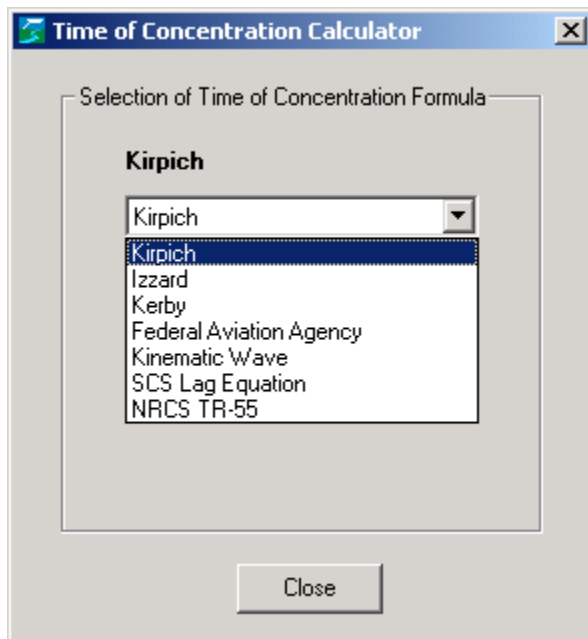
$$T_{oc} = \frac{L_{oc} n_{oc} P_w^{2/3}}{89.4 A_c^{2/3} S_{oc}^{1/2}}$$

where  $L_{oc}$  = open channel flow length (ft),  $n_{oc}$  = Manning's roughness coefficient for open channel flow,  $P_w$  = wetted perimeter (ft),  $A_c$  = cross sectional area (ft<sup>2</sup>), and  $S_{oc}$  = slope of hydraulic grade line (channel slope, ft/ft).

Total time of concentration (min),  $T_c$

$$T_c = T_{st} + T_{sc} + T_{oc}$$

Application Conditions: Movement of the surface water in a watershed is characterized by three major types of flow: sheet flow, shallow concentrated flow, and open channel flow; after a maximum of 300 ft, sheet flow becomes shallow concentrated flow; steady uniform sheet flow.



**Kirpich** ✕

Kirpich Tc (min)

Equations 
$$T_c = 0.0078 \frac{L^{0.77}}{S^{0.385}}$$

L = length of flow (ft)  
S = slope (ft/ft)

Application Conditions  
Small rural basins (1.2 - 112 acres);  
Steep slopes (3% - 10%);  
Overland flow on bare soil;  
For overland flow on concrete or asphalt surfaces, multiply by 0.4;  
For concrete channels, multiply by 0.2.

L (ft)

S (ft/ft)

Time of Concentration (min)

**Izzard** ✕

Izzard Tc (min)

Equations 
$$T_c = \frac{41.025(0.0007i + c_r)L^{1/2}}{S^{1/2}i^{1/2}}$$

i = rainfall intensity (in/hr)  
c<sub>r</sub> = retardation coefficient  
L = length of flow (ft)  
S = slope (ft/ft)

Application Conditions  
Overland flow on roadway and turf surface;  
iL < 500 in. ft/hr;  
Requires iteration;  
c<sub>r</sub> = 0.007 for very smooth pavement (asphalt);  
c<sub>r</sub> = 0.0075 for tar and sand pavement;  
c<sub>r</sub> = 0.012 for concrete pavement;  
c<sub>r</sub> = 0.06 for dense turf.

i (in/hr)

c<sub>r</sub>

L (ft)

S (ft/ft)

Time of Concentration (min)

**Kerby** ✕

Kerby Tc (min)

Equations 
$$T_c = 0.8262 \frac{L^{0.467} n^{0.467}}{S^{0.2335}}$$

L = length of flow (ft)  
S = mean slope of the basin (ft/ft)  
n = Manning roughness coefficient or retardation coefficient

Application Conditions  
Overland flow on small watersheds (< 4.047 ha or 10 ac);  
L < 1000 ft;  
n = 0.02 for smooth pavement;  
n = 0.3 for poor grass;  
n = 0.4 for average grass;  
n = 0.8 for dense grass.

L (ft)

S (ft/ft)

n

Time of Concentration (min)

**Federal Aviation Agency** ✕

Federal Aviation Agency Tc (min)

Equations 
$$T_c = \frac{0.3884(1.1 - C)L^{0.5}}{S^{0.333}}$$

L = length of overland flow (ft)  
S = average overland slope (ft/ft)  
C = rational runoff coefficient

Application Conditions  
Overland flow;  
Frequently used for urban basins.

L (ft)

S (ft/ft)

C

Time of Concentration (min)

**Kinematic Wave**

Kinematic Wave Tc (min)

Equations 
$$T_c = \frac{0.93L^{0.6}n^{0.6}}{i^{0.4}S^{0.3}}$$

L = length of overland flow (ft)  
 S = average overland slope (ft/ft)  
 n = Manning roughness coefficient for overland flow  
 i = rainfall intensity (in/hr)

Application Conditions: Overland flow; L < 300 ft; Requires iteration.

L (ft)

S (ft/ft)

n

i (in/hr)

Time of Concentration (min)

Compute

Close

**SCS Lag Equation**

SCS Lag Equation Tc (min)

Equations 
$$T_c = \frac{L^{0.8} \left( \frac{1000}{CN} - 9 \right)^{0.7}}{189.62S^{0.5}}$$

L = watershed hydraulic length (ft)  
 S = average watershed slope (ft/ft)  
 CN = runoff curve number

Application Conditions: Agricultural watersheds; small urban basins (< 2000 acres); Assuming Tc = 1.67 TL.

L (ft)

S (ft/ft)

CN

Time of Concentration (min)

Lag Time (min)

Compute

Close

NRCS TR-55

NRCS TR-55 T<sub>c</sub> (min)

Equations

$$T_{st} = \frac{0.42(n_{st}L_{st})^{0.8}}{P_2^{0.5}S_{st}^{0.4}}$$

$$T_{sc} = \frac{L_{sc}}{60C_cS_{sc}^{0.5}}$$

$$T_{oc} = \frac{L_{oc}n_{oc}P_w^{1/2}}{89.4A_c^{1/2}S_{oc}^{1/2}}$$

Remarks  
Notations

L<sub>sc</sub> = shallow concentrated flow length (ft)  
C<sub>c</sub> = channel type coefficient (unpaved channel: C<sub>c</sub> = 16.1345; paved channel: C<sub>c</sub> = 20.3282)  
S<sub>sc</sub> = slope of hydraulic grade line (watercourse slope, ft/ft)  
L<sub>oc</sub> = open channel flow length (ft)  
n<sub>oc</sub> = Manning's roughness coefficient for open channel flow

Sheet Flow T<sub>st</sub> (min)

L<sub>st</sub> (ft)  n<sub>st</sub>  Sheet Flow T<sub>st</sub> (min)

S<sub>st</sub> (ft/ft)  P<sub>2</sub> (in)  Compute

Shallow Concentrated Flow T<sub>sc</sub> (min)

L<sub>sc</sub> (ft)  C<sub>c</sub>  Shallow Concentrated Flow T<sub>sc</sub> (min)

S<sub>sc</sub> (ft/ft)  Compute

Open Channel Flow T<sub>oc</sub> (min)

L<sub>oc</sub> (ft)  n<sub>oc</sub>  Open Channel Flow T<sub>oc</sub> (min)

S<sub>oc</sub> (ft/ft)  P<sub>w</sub> (ft)  Compute

A<sub>c</sub> (ft<sup>2</sup>)

**Time of Concentration (T<sub>st</sub> + T<sub>sc</sub> + T<sub>oc</sub>) (min)**

Close

### 10.3 24-Hour Rainfall Generator

For a designed rainfall (2-year, 5-year, 10-year, 25-year, 50-year, or 100-year), the USDA-NRCS (SCS) 24-rainfall distributions (USDA, 1986) can be applied to generate the corresponding rainfall time series. In this tool, three parameters need to be specified, which include the number of time points for 24 hours, type of the rainfall distribution (I, II, III, or IA), and the total 24-hour rainfall. The relevant information can be easily accessed via buttons on the interface of the tool. The calculated 24-hour rainfall can also be exported to an EXCEL file.

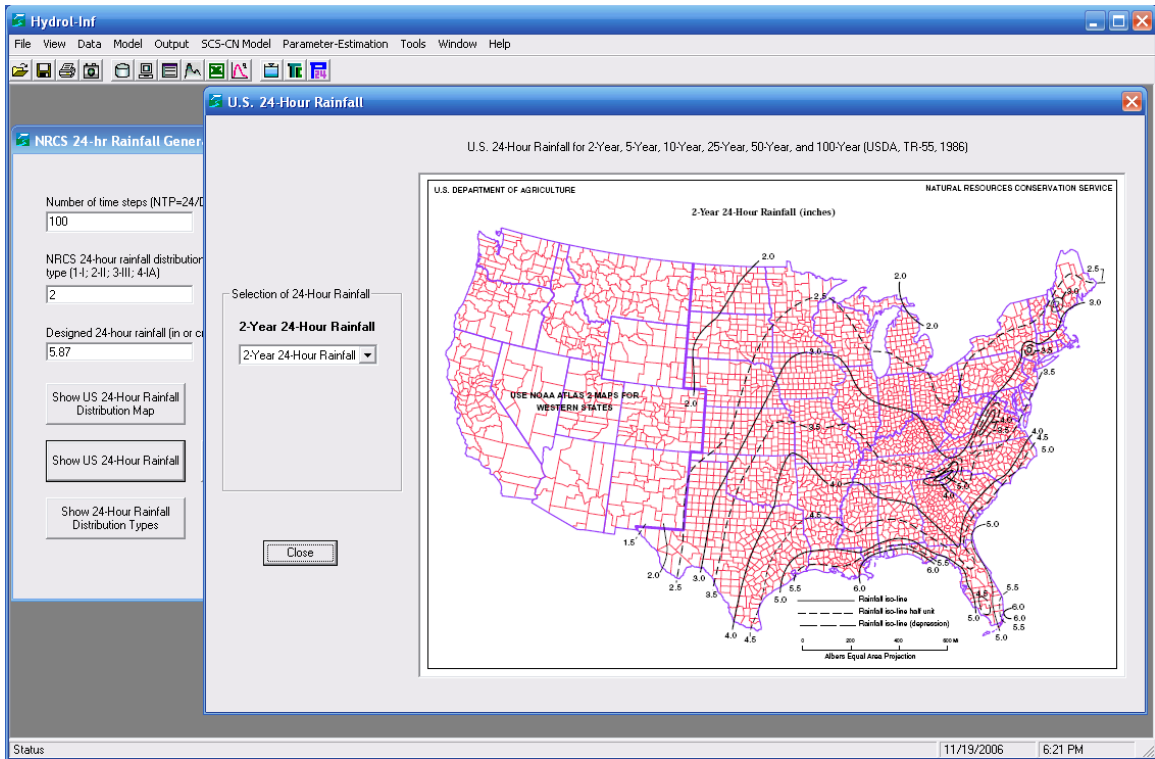
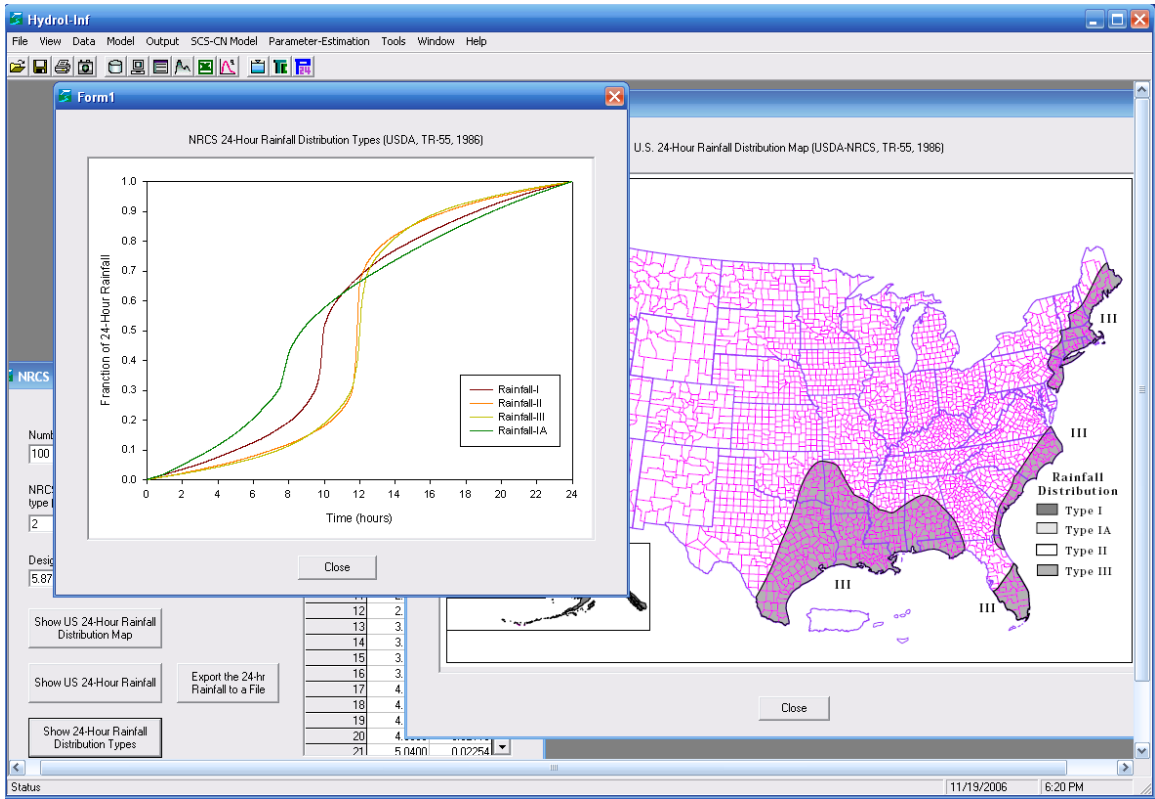
**NRCS 24-hr Rainfall Generator**

Number of time steps (NTP=24/DT)

NRCS 24-hour rainfall distribution type (1-I; 2-II; 3-III; 4-IA)

Designed 24-hour rainfall (in or cm)

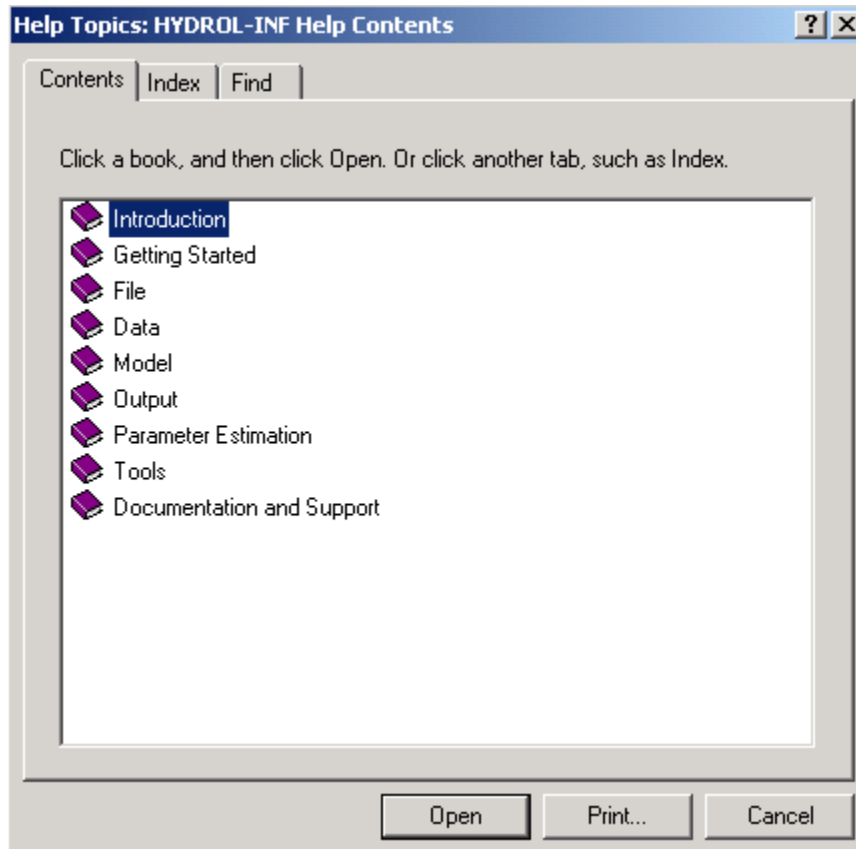
Step	Time(hr)	Rainfall
1	0.2400	0.01409
2	0.4800	0.01468
3	0.7200	0.01479
4	0.9600	0.01550
5	1.2000	0.01550
6	1.4400	0.01608
7	1.6800	0.01608
8	1.9200	0.01679
9	2.1600	0.01691
10	2.4000	0.01749
11	2.6400	0.01749
12	2.8800	0.01796
13	3.1200	0.01831
14	3.3600	0.01867
15	3.6000	0.01914
16	3.8400	0.01914
17	4.0800	0.01972
18	4.3200	0.02043
19	4.5600	0.02113
20	4.8000	0.02113
21	5.0400	0.02254



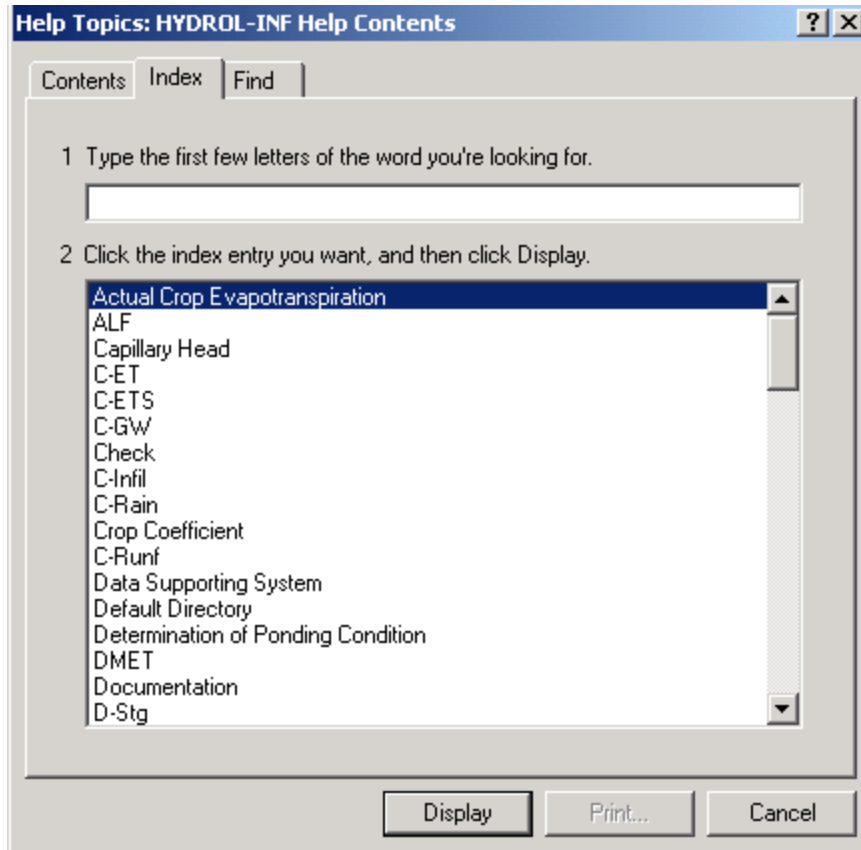
## 11. Help and Documentation

### 11.1 Help System

The help system covers all major topics associated with use of the model, input data and parameter estimation, as well as hydrologic tools and documentation. Users can find the answers to most of their questions from the help system.

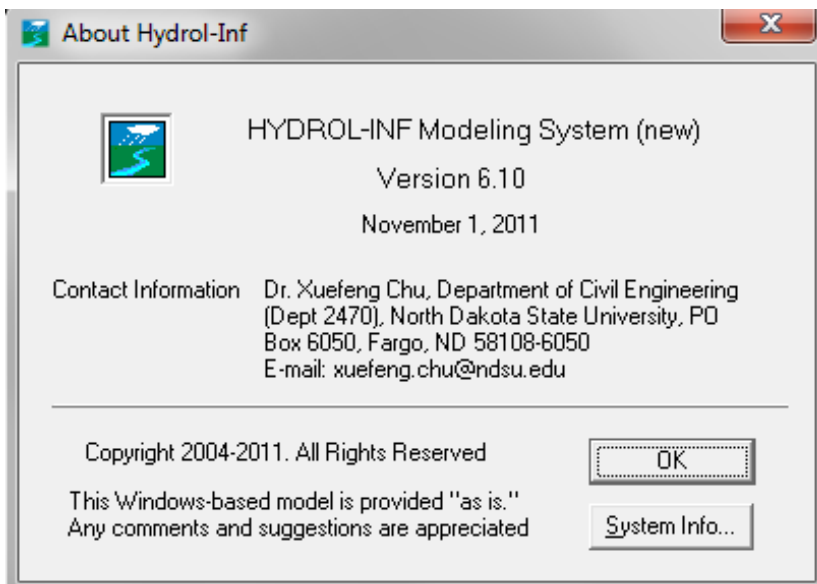
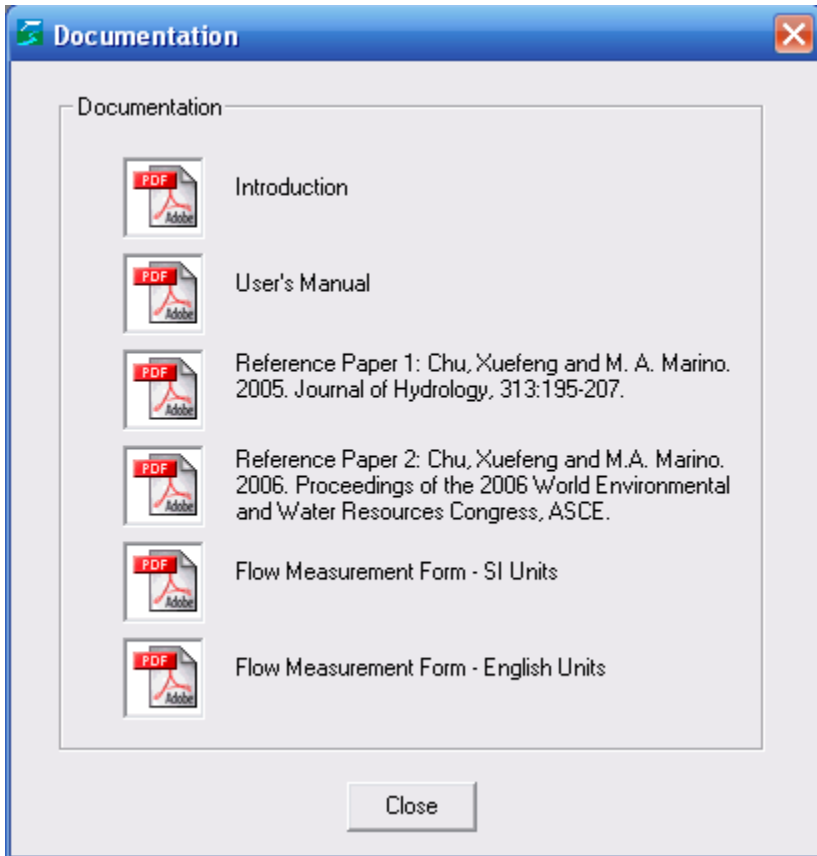






## 11.2 Documentation and Support

This User's Manual is the primary documentation. To help users understand the underlying theoretical background, relevant papers also are included in this Windows-based model. Additionally, users can visit our Hydrol-Inf website to check any updated information. Limited technical support can be available via e-mail (xuefeng.chu@ndsu.edu). Any comments and improvement suggestions on HYDROL-INF are greatly appreciated.



## 12 References

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## Appendix 1. Tables

Table 1 Saturated Hydraulic Conductivity KS (cm/hr)

Soil Texture Class	KS (cm/hr) <sup>a</sup>	KS (cm/hr) <sup>b, c</sup>
Sand	29.7	23.56
Loamy Sand	14.59	5.98
Sandy Loam	4.42	2.18
Loam	1.04	1.32
Silt	0.25	
Silt Loam	0.45	0.68
Sandy Clay Loam	1.31	0.30
Clay Loam	0.26	0.20
Silty Clay Loam	0.07	0.20
Sandy Clay	0.12	0.12
Silty Clay	0.02	0.10
Clay	0.20	0.06

<sup>a</sup> Carsel and Parrish, 1988.

<sup>b</sup> Rawls and Brakensiek, 1983.

<sup>c</sup> Maidment, 1993.

Table 2 Capillary Head HWT (cm)

Soil Texture Class	HWT (cm) <sup>a, b</sup>
Sand	4.95 (0.97-25.36)
Loamy Sand	6.13 (1.35-27.94)
Sandy Loam	11.01 (2.67-45.47)
Loam	8.89 (1.33-59.38)
Silt Loam	16.68 (2.92-95.39)
Sandy Clay Loam	21.85 (4.42-108.0)
Clay Loam	20.88 (4.79-91.10)
Silty Clay Loam	27.30 (5.67-131.50)
Sandy Clay	23.90 (4.08-140.2)
Silty Clay	29.22 (6.13-139.4)
Clay	31.63 (6.39-156.5)

<sup>a</sup> Rawls and Brakensiek, 1983.

<sup>b</sup> Maidment, 1993.

Table 3 Saturated Water Content WS (cm<sup>3</sup>/cm<sup>3</sup>)

Soil Texture Class	WS (cm <sup>3</sup> /cm <sup>3</sup> ) <sup>a</sup>
Sand	0.43
Loamy Sand	0.41
Sandy Loam	0.41

Loam	0.43
Silt	0.46
Silt Loam	0.45
Sandy Clay Loam	0.39
Clay Loam	0.41
Silty Clay Loam	0.43
Sandy Clay	0.38
Silty Clay	0.36
Clay	0.38

<sup>a</sup> Carsel and Parrish, 1988.

Table 4 Residual Water Content WR (cm<sup>3</sup>/cm<sup>3</sup>)

Soil Texture Class	WR (cm <sup>3</sup> /cm <sup>3</sup> ) <sup>a</sup>
Sand	0.045
Loamy Sand	0.057
Sandy Loam	0.065
Loam	0.078
Silt	0.034
Silt Loam	0.067
Sandy Clay Loam	0.100
Clay Loam	0.095
Silty Clay Loam	0.089
Sandy Clay	0.100
Silty Clay	0.070
Clay	0.068

<sup>a</sup> Carsel and Parrish, 1988.

Table 5 Soil Water Retention Parameter n VN <sup>a</sup>

Soil Type	VN
Sand	2.68
Loamy Sand	2.28
Sandy Loam	1.89
Loam	1.56
Silt	1.37
Silt Loam	1.41
Sandy Clay Loam	1.48
Clay Loam	1.31
Silty Clay Loam	1.23
Sandy Clay	1.23
Silty Clay	1.09
Clay	1.09

<sup>a</sup> Carsel and Parrish, 1988.

Table 6 Soil Water Retention Parameter  $\alpha$  ALF (1/cm) <sup>a</sup>

Soil Type	$\alpha$ (1/cm) <sup>a</sup>
Sand	0.145
Loamy Sand	0.124
Sandy Loam	0.075
Loam	0.036
Silt	0.016
Silt Loam	0.020
Sandy Clay Loam	0.059
Clay Loam	0.019
Silty Clay Loam	0.010
Sandy Clay	0.027
Silty Clay	0.005
Clay	0.008

<sup>a</sup> Carsel and Parrish, 1988.

Table 7 Field Capacity FC (cm<sup>3</sup>/cm<sup>3</sup>) <sup>a</sup>

Soil Texture Class	Textural Properties (%)			FC (Water Retained at -0.33 Bar Tension)
	Sand	Silt	Clay	
Sand	85-100	0-15	0-10	0.091 (0.018-0.164)
Loamy Sand	70-90	0-30	0-15	0.125 (0.060-0.190)
Sandy Loam	45-85	0-50	0-20	0.207 (0.126-0.288)
Loam	25-50	28-50	8-28	0.270 (0.195-0.345)
Silt Loam	0-50	50-100	8-28	0.330 (0.258-0.402)
Sandy Clay Loam	45-80	0-28	20-35	0.257 (0.186-0.324)
Clay Loam	20-45	15-55	28-50	0.318 (0.250-0.386)
Silty Clay Loam	0-20	40-73	28-40	0.366 (0.304-0.428)
Sandy Clay	45-65	0-20	35-55	0.339 (0.245-0.433)
Silty Clay	0-20	40-60	40-60	0.387 (0.332-0.442)
Clay	0-45	0-40	40-100	0.396 (0.326-0.466)

<sup>a</sup> Rawls et al., 1982.

Table 8 Wilting Point WP (cm<sup>3</sup>/cm<sup>3</sup>) <sup>a</sup>

Soil Texture Class	Textural Properties (%)			WP (Water Retained at -15.0 Bar Tension)
	Sand	Silt	Clay	
Sand	85-100	0-15	0-10	0.033 (0.007-0.059)
Loamy Sand	70-90	0-30	0-15	0.055 (0.019-0.091)
Sandy Loam	45-85	0-50	0-20	0.095 (0.031-0.159)

Loam	25-50	28-50	8-28	0.117 (0.069-0.165)
Silt Loam	0-50	50-100	8-28	0.133 (0.078-0.188)
Sandy Clay Loam	45-80	0-28	20-35	0.148 (0.085-0.211)
Clay Loam	20-45	15-55	28-50	0.197 (0.115-0.279)
Silty Clay Loam	0-20	40-73	28-40	0.208 (0.138-0.278)
Sandy Clay	45-65	0-20	35-55	0.239 (0.162-0.316)
Silty Clay	0-20	40-60	40-60	0.250 (0.193-0.307)
Clay	0-45	0-40	40-100	0.272 (0.208-0.336)

<sup>a</sup> Rawls et al., 1982.

Table 9 Crop Coefficients and Mean Maximum Plant Heights <sup>a</sup>

Crop	Kc ini <sup>1</sup>	Kc mid	Kc end	Maximum Crop Height h (m)
a. Small Vegetables	0.7	1.05	0.95	
Broccoli		1.05	0.95	0.3
Brussel Sprouts		1.05	0.95	0.4
Cabbage		1.05	0.95	0.4
Carrots		1.05	0.95	0.3
Cauliflower		1.05	0.95	0.4
Celery		1.05	1.00	0.6
Garlic		1.00	0.70	0.3
Lettuce		1.00	0.95	0.3
Onions - dry		1.05	0.75	0.4
- green		1.00	1.00	0.3
- seed		1.05	0.80	0.5
Spinach		1.00	0.95	0.3
Radish		0.90	0.85	0.3
b. Vegetables – Solanum Family ( <i>Solanaceae</i> )	0.6	1.15	0.80	
Egg Plant		1.05	0.90	0.8
Sweet Peppers (bell)		1.05 <sup>2</sup>	0.90	0.7
Tomato		1.15 <sup>2</sup>	0.70-0.90	0.6
c. Vegetables – Cucumber Family ( <i>Cucurbitaceae</i> )	0.5	1.00	0.80	
Cantaloupe	0.5	0.85	0.60	0.3

Cucumber - Fresh Market	0.6	1.00 <sup>2</sup>	0.75	0.3
- Machine harvest	0.5	1.00	0.90	0.3
Pumpkin, Winter Squash		1.00	0.80	0.4
Squash, Zucchini		0.95	0.75	0.3
Sweet Melons		1.05	0.75	0.4
Watermelon	0.4	1.00	0.75	0.4
d. Roots and Tubers	0.5	1.10	0.95	
Beets, table		1.05	0.95	0.4
Cassava - year 1	0.3	0.80 <sup>3</sup>	0.30	1.0
- year 2	0.3	1.10	0.50	1.5
Parsnip	0.5	1.05	0.95	0.4
Potato		1.15	0.75 <sup>4</sup>	0.6
Sweet Potato		1.15	0.65	0.4
Turnip (and Rutabaga)		1.10	0.95	0.6
Sugar Beet	0.35	1.20	0.70 <sup>5</sup>	0.5
e. Legumes ( <i>Leguminosae</i> )	0.4	1.15	0.55	
Beans, green	0.5	1.05 <sup>2</sup>	0.90	0.4
Beans, dry and Pulses	0.4	1.15 <sup>2</sup>	0.35	0.4
Chick pea		1.00	0.35	0.4
Fababean (broad bean) - Fresh		1.15 <sup>2</sup>	1.10	0.5
- Dry/Seed	0.5	1.15	0.30	0.5
Grabanzo	0.4	1.15	0.35	0.8
Green Gram and Cowpeas		1.05	0.60-0.35 <sup>6</sup>	0.4
Groundnut (Peanut)		1.15	0.60	0.4
Lentil		1.10	0.30	0.5
Peas - Fresh		1.15 <sup>2</sup>	1.10	0.5
- Dry/Seed	0.5	1.15	0.30	0.5
Soybeans		1.15	0.50	0.5-1.0
f. Perennial Vegetables (with winter dormancy and initially bare or mulched soil)	0.5	1.00	0.80	
Artichokes	0.5	1.00	0.95	0.7
Asparagus	0.5	0.95 <sup>7</sup>	0.30	0.2-0.8
Mint	0.6	1.15	1.10	0.6-0.8
Strawberries	0.4	0.85	0.75	0.2
g. Fibre Crops	0.35			



Cotton		1.15-1.2	0.70-0.50	1.2-1.5
Flax		1.10	0.25	1.2
Sisal <sup>8</sup>		0.4-0.7	0.4-0.7	1.5
h. Oil Crops	0.35	1.15	0.35	
Castorbean ( <i>Ricinus</i> )		1.15	0.55	0.3
Rapeseed, Canola		1.00-1.15 <sup>9</sup>	0.35	0.6
Safflower		1.00-1.15 <sup>9</sup>	0.25	0.8
Sesame		1.10	0.25	1.0
Sunflower		1.00-1.15 <sup>9</sup>	0.35	2.0
i. Cereals	0.3	1.15	0.4	
Barley		1.15	0.25	1
Oats		1.15	0.25	1
Spring Wheat		1.15	0.25-0.4 <sup>10</sup>	1
Winter Wheat - with frozen soils	0.4	1.15	0.25-0.4 <sup>10</sup>	1
- with non-frozen soils	0.7	1.15	0.25-0.4 <sup>10</sup>	1
Maize, Field (grain) ( <i>field corn</i> )		1.20	0.60,0.35 <sup>11</sup>	2
Maize, Sweet ( <i>sweet corn</i> )		1.15	1.05 <sup>12</sup>	1.5
Millet		1.00	0.30	1.5
Sorghum - grain		1.00-1.10	0.55	1-2
- sweet		1.20	1.05	2-4
Rice	1.05	1.20	0.90-0.60	1
j. Forages				
Alfalfa Hay - averaged cutting effects	0.40	0.95	0.90	0.7
- individual cutting periods	0.40	1.20	1.15	0.7
- for seed	0.40	0.50	0.50	0.7
Bermuda hay - averaged cutting effects	0.55	1.00	0.85	0.35
- Spring crop for seed	0.35	0.90	0.65	0.40
Clover hay, Berseem				
- averaged cutting effects	0.40	0.90 <sup>13</sup>	0.85	0.6
- individual cutting periods	0.40 <sup>14</sup>	1.15 <sup>14</sup>	1.10 <sup>14</sup>	0.6
Rye Grass hay - averaged cutting effects	0.95	1.05	1.00	0.3
Sudan Grass hay (annual)				
- averaged cutting effects	0.50	0.90 <sup>14</sup>	0.85	1.2
- individual cutting periods	0.50 <sup>14</sup>	1.15 <sup>14</sup>	1.10 <sup>14</sup>	1.2
Grazing Pasture - Rotated Grazing	0.40	0.85-1.05	0.85	0.15-0.30
- Extensive Grazing	0.30	0.75	0.75	0.10

Turf grass - cool season <sup>15</sup>	0.90	0.95	0.95	0.10
- warm season <sup>15</sup>	0.80	0.85	0.85	0.10
k. Sugar Cane	0.40	1.25	0.75	3
l. Tropical Fruits and Trees				
Banana - 1 <sup>st</sup> year	0.50	1.10	1.00	3
- 2 <sup>nd</sup> year	1.00	1.20	1.10	4
Cacao	1.00	1.05	1.05	3
Coffee - bare ground cover	0.90	0.95	0.95	2-3
- with weeds	1.05	1.10	1.10	2-3
Date Palms	0.90	0.95	0.95	8
Palm Trees	0.95	1.00	1.00	8
Pineapple <sup>16</sup> - bare soil	0.50	0.30	0.30	0.6-1.2
- with grass cover	0.50	0.50	0.50	0.6-1.2
Rubber Trees	0.95	1.00	1.00	10
Tea - non-shaded	0.95	1.00	1.00	1.5
- shaded <sup>17</sup>	1.10	1.15	1.15	2
m. Grapes and Berries				
Berries (bushes)	0.30	1.05	0.50	1.5
Grapes - Table or Raisin	0.30	0.85	0.45	2
- Wine	0.30	0.70	0.45	1.5-2
Hops	0.3	1.05	0.85	5
n. Fruit Trees				
Almonds, no ground cover	0.40	0.90	0.65 <sup>18</sup>	5
Apples, Cherries, Pears <sup>19</sup>				
-no ground cover, killing frost	0.45	0.95	0.70 <sup>18</sup>	4
-no ground cover, no frosts	0.60	0.95	0.75 <sup>18</sup>	4
-active ground cover, killing frost	0.50	1.20	0.95 <sup>18</sup>	4
-active ground cover, no frosts	0.80	1.20	0.85 <sup>18</sup>	4
Apricots, Peaches, Stone Fruit <sup>19, 20</sup>				
-no ground cover, killing frost	0.45	0.90	0.65 <sup>18</sup>	3
-no ground cover, no frosts	0.55	0.90	0.65 <sup>18</sup>	3
-active ground cover, killing frost	0.50	1.15	0.90 <sup>18</sup>	3
-active ground cover, no frosts	0.80	1.15	0.85 <sup>18</sup>	3
Avocado, no ground cover	0.60	0.85	0.75	3
Citrus, no ground cover <sup>21</sup>				
- 70% canopy	0.70	0.65	0.70	4
- 50% canopy	0.65	0.60	0.65	3
- 20% canopy	0.50	0.45	0.55	2

Citrus, with active ground cover or weeds <sup>22</sup>				
- 70% canopy	0.75	0.70	0.75	4
- 50% canopy	0.80	0.80	0.80	3
- 20% canopy	0.85	0.85	0.85	2
Conifer Trees <sup>23</sup>	1.00	1.00	1.00	10
Kiwi	0.40	1.05	1.05	3
Olives (40 to 60% ground coverage by canopy) <sup>24</sup>	0.65	0.70	0.70	3-5
Pistachios, no ground cover	0.40	1.10	0.45	3-5
Walnut Orchard <sup>19</sup>	0.50	1.10	0.65 <sup>18</sup>	4-5
o. Wetlands – temperate climate				
Cattails, Bulrushes, killing frost	0.30	1.20	0.30	2
Cattails, Bulrushes, no frost	0.60	1.20	0.60	2
Short Veg., no frost	1.05	1.10	1.10	0.3
Reed Swamp, standing water	1.00	1.20	1.00	1-3
Reed Swamp, moist soil	0.90	1.20	0.70	1-3
p. Special				
Open Water, < 2 m depth or in subhumid climates or tropics		1.05	1.05	
Open Water, > 5 m depth, clear of turbidity, temperate climate		0.65 <sup>25</sup>	1.25 <sup>25</sup>	

1. These are general values for Kc ini under typical irrigation management and soil wetting. For frequent wettings such as with high frequency sprinkle irrigation or daily rainfall, these values may increase substantially and may approach 1.0 to 1.2. Kc ini is a function of wetting interval and potential evaporation rate during the initial and development periods and is more accurately estimated using Figures 29 and 30, or Equation 7-3 in Annex 7, or using the dual Kcb ini + Ke.
2. Beans, Peas, Legumes, Tomatoes, Peppers and Cucumbers are sometimes grown on stalks reaching 1.5 to 2 meters in height. In such cases, increased Kc values need to be taken. For green beans, peppers and cucumbers, 1.15 can be taken, and for tomatoes, dry beans and peas, 1.20. Under these conditions h should be increased also.
3. The midseason values for cassava assume non-stressed conditions during or following the rainy season. The Kc end values account for dormancy during the dry season.
4. The Kc end value for potatoes is about 0.40 for long season potatoes with vine kill.
5. This Kc end value is for no irrigation during the last month of the growing season. The Kc end value for sugar beets is higher, up to 1.0, when irrigation or significant rain occurs during the last month.
6. The first Kc end is for harvested fresh. The second value is for harvested dry.

7. The  $K_c$  for asparagus usually remains at  $K_c$  ini during harvest of the spears, due to sparse ground cover. The  $K_c$  mid value is for following regrowth of plant vegetation following termination of harvest of spears.
8.  $K_c$  for sisal depends on the planting density and water management (e.g., intentional moisture stress).
9. The lower values are for rainfed crops having less dense plant populations.
10. The higher value is for hand-harvested crops.
11. The first  $K_c$  end value is for harvest at high grain moisture. The second  $K_c$  end value is for harvest after complete field drying of the grain (to about 18% moisture, wet mass basis).
12. If harvested fresh for human consumption. Use  $K_c$  end for field maize if the sweet maize is allowed to mature and dry in the field.
13. This  $K_c$  mid coefficient for hay crops is an overall average  $K_c$  mid coefficient that averages  $K_c$  for both before and following cuttings. It is applied to the period following the first development period until the beginning of the last late season period of the growing season.
14. These  $K_c$  coefficients for hay crops represent immediately following cutting; at full cover; and immediately before cutting, respectively. The growing season is described as a series of individual cutting periods (Figure 35).
15. Cool season grass varieties include dense stands of bluegrass, ryegrass, and fescue. Warm season varieties include bermuda grass and St. Augustine grass. The 0.95 values for cool season grass represent a 0.06 to 0.08 m mowing height under general turf conditions. Where careful water management is practiced and rapid growth is not required,  $K_c$ 's for turf can be reduced by 0.10.
16. The pineapple plant has very low transpiration because it closes its stomates during the day and opens them during the night. Therefore, the majority of  $ET_c$  from pineapple is evaporation from the soil. The  $K_c$  mid  $<$   $K_c$  ini since  $K_c$  mid occurs during full ground cover so that soil evaporation is less. Values given assume that 50% of the ground surface is covered by black plastic mulch and that irrigation is by sprinkler. For drip irrigation beneath the plastic mulch,  $K_c$ 's given can be reduced by 0.10.
17. Includes the water requirements of the shade trees.
18. These  $K_c$  end values represent  $K_c$  prior to leaf drop. After leaf drop,  $K_c$  end  $\approx$  0.20 for bare, dry soil or dead ground cover and  $K_c$  end  $\approx$  0.50 to 0.80 for actively growing ground cover (consult Chapter 11).
19. Refer to Eq. 94, 97 or 98 and footnotes 21 and 22 for estimating  $K_c$  for immature stands.
20. Stone fruit category applies to peaches, apricots, pears, plums and pecans.
21. These  $K_c$  values can be calculated from Eq. 98 for  $K_c$  min = 0.15 and  $K_c$  full = 0.75, 0.70 and 0.75 for the initial, mid season and end of season periods, and  $f_c$  eff =  $f_c$  where  $f_c$  = fraction of ground covered by tree canopy (e.g., the sun is presumed to be directly overhead). The values listed correspond with those in Doorenbos and Pruitt (1977) and with more recent measurements. The midseason value is lower than initial and ending values due to the effects of stomatal closure during periods of peak  $ET$ . For humid and subhumid climates where there is less stomatal control by citrus,

- values for  $K_c$  ini,  $K_c$  mid, and  $K_c$  end can be increased by 0.1 - 0.2, following Rogers et al. (1983).
22. These  $K_c$  values can be calculated as  $K_c = f_c K_c \text{ ngc} + (1 - f_c) K_c \text{ cover}$  where  $K_c \text{ ngc}$  is the  $K_c$  of citrus with no active ground cover (calculated as in footnote 21),  $K_c \text{ cover}$  is the  $K_c$  for the active ground cover (0.95), and  $f_c$  is defined in footnote 21. The values listed correspond with those in Doorenbos and Pruitt (1977) and with more recent measurements. Alternatively,  $K_c$  for citrus with active ground cover can be estimated directly from Eq. 98 by setting  $K_c \text{ min} = K_c \text{ cover}$ . For humid and subhumid climates where there is less stomatal control by citrus, values for  $K_c$  ini,  $K_c$  mid, and  $K_c$  end can be increased by 0.1 - 0.2, following Rogers et al. (1983). For non-active or only moderately active ground cover (active indicates green and growing ground cover with LAI > about 2 to 3),  $K_c$  should be weighted between  $K_c$  for no ground cover and  $K_c$  for active ground cover, with the weighting based on the "greenness" and approximate leaf area of the ground cover.
  23. Conifers exhibit substantial stomatal control due to reduced aerodynamic resistance. The  $K_c$  can easily reduce below the values presented, which represent well-watered conditions for large forests.
  24. These coefficients represent about 40 to 60% ground cover. Refer to Eq. 98 and footnotes 21 and 22 for estimating  $K_c$  for immature stands. In Spain, Pastor and Orgaz (1994) have found the following monthly  $K_c$ 's for olive orchards having 60% ground cover: 0.50, 0.50, 0.65, 0.60, 0.55, 0.50, 0.45, 0.45, 0.55, 0.60, 0.65, 0.50 for months January through December. These coefficients can be invoked by using  $K_c \text{ ini} = 0.65$ ,  $K_c \text{ mid} = 0.45$ , and  $K_c \text{ end} = 0.65$ , with stage lengths = 30, 90, 60 and 90 days, respectively for initial, development, midseason and late season periods, and sing  $K_c$  during the winter ("off season") in December to February = 0.50.
  25. These  $K_c$ 's are for deep water in temperate latitudes where large temperature changes in the water body occur during the year, and initial and peak period evaporation is low as radiation energy is absorbed into the deep water body. During fall and winter periods ( $K_c \text{ end}$ ), heat is released from the water body that increases the evaporation above that for grass. Therefore,  $K_c \text{ mid}$  corresponds to the period when the water body is gaining thermal energy and  $K_c \text{ end}$  when releasing thermal energy. These  $K_c$ 's should be used with caution.

<sup>a</sup> Allen et al., 1998.

## Appendix 2. Figures

Figure 1 Field Capacity (Rawls and Brakensiek, 1983; Carsel et al., 2003)

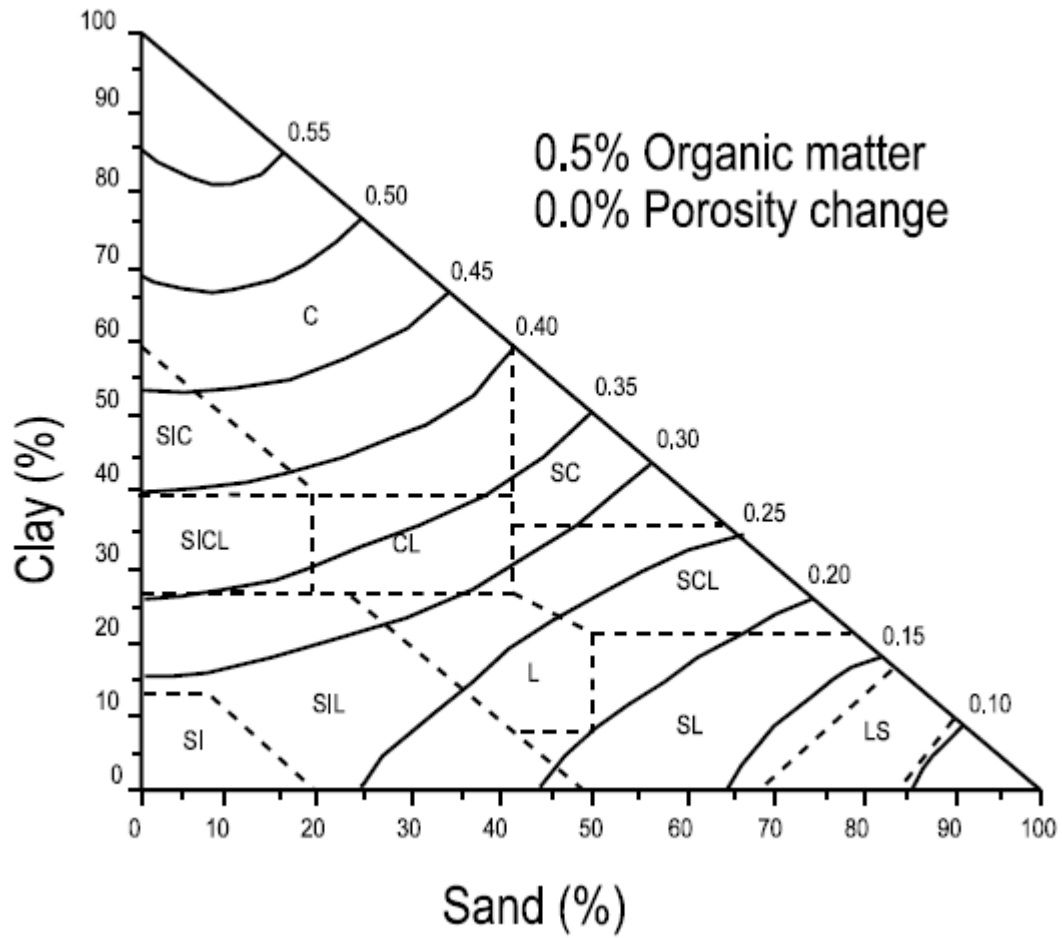
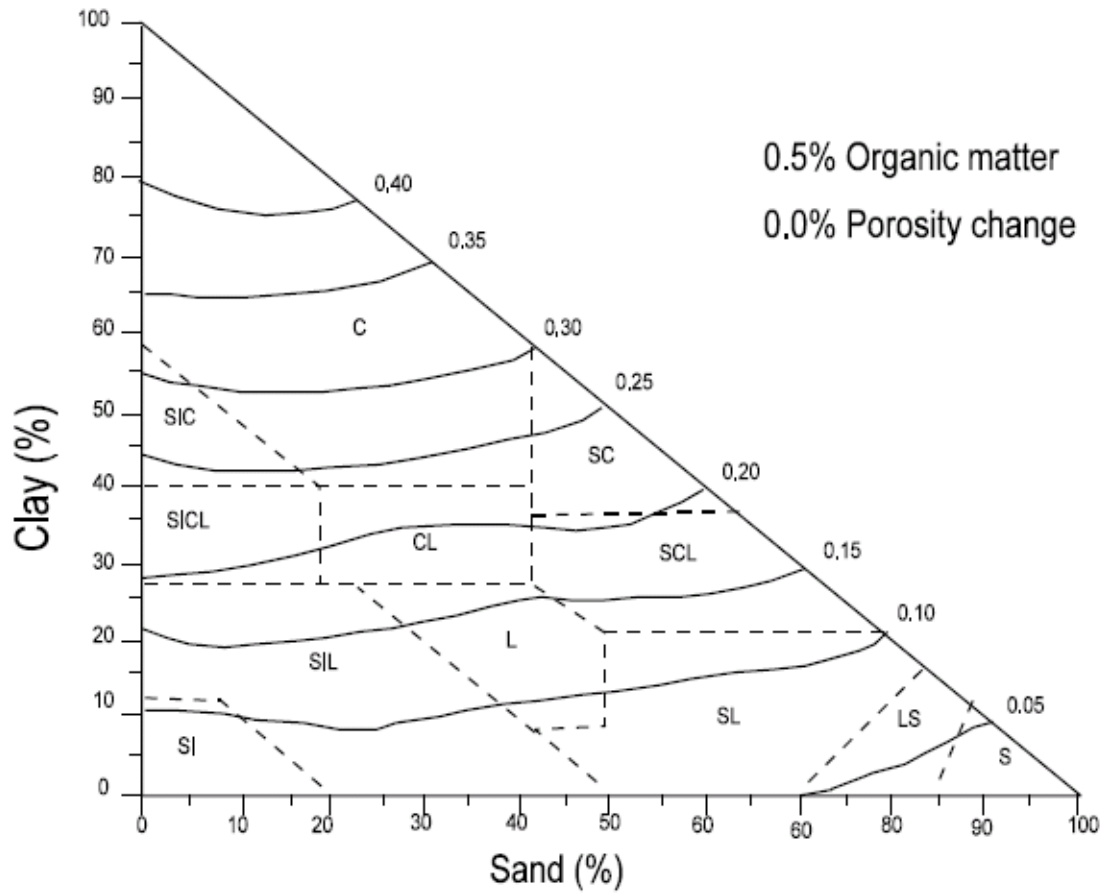


Figure 2 Wilting Point (Rawls and Brakensiek, 1983; Carsel et al., 2003)



### Appendix 3. List of Input Data

AHA: Watershed area (ha)  
ALF(I): Soil retention parameter (1/cm)  
DMET: Maximum ET depth in soil (cm)  
DT: Size of a time step (hr)  
FC(I): Field capacity ( $\text{cm}^3/\text{cm}^3$ )  
ET0(I): Potential evapotranspiration rate (cm/hr)  
HWT(I): Capillary head (suction) (cm)  
IMP: Percentage of directly-connected impervious area (%)  
IU: Index of the UH method (1: SCS UH; 2: Clark UH)  
KE(I): Effective hydraulic conductivity (cm/hr)  
KBC(I): Crop coefficient  
KS(I): Saturated hydraulic conductivity (cm/hr)  
NC(I): Number of computation cells for each soil layer  
NL: Number of soil layers  
NT: Number of time steps  
QB0: Initial baseflow ( $\text{m}^3/\text{s}$ )  
RAINS(I): Rainfall intensity (cm/hr)  
RC: Basin storage coefficient in the Clark UH (hr)  
RB: Baseflow recession constant  
RTHRE: Threshold value (ratio to the peak)  
SSMAX: Surface storage capacity (cm)  
TC: Time of concentration (hr)  
VN(I): Soil water retention parameter  
W0(I): Initial volumetric water content ( $\text{cm}^3/\text{cm}^3$ )  
WP(I): Wilting point ( $\text{cm}^3/\text{cm}^3$ )  
WR(I): Volumetric residual water content ( $\text{cm}^3/\text{cm}^3$ )  
WS(I): Volumetric saturated water content ( $\text{cm}^3/\text{cm}^3$ )  
ZNL(I): Thickness of each soil layer (cm)